## IN-STREAM HABITAT COMPLEXING 1993-1995 -PILOT TESTING-

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#### ABSTRACT

The Nechako River In-Stream Habitat Complexing Project began in 1988 with pilot tests conducted to increase the complexity of juvenile chinook habitat prior to the implementation of the Long-Term Flow Regime of the Kemano Completion Project. Its immediate objectives were to design, test and monitor habitat complex structures specific to the Nechako River. Different habitat complex designs were constructed and monitored between 1988 and 1992. No new complexes were constructed after 1992. This report documents the work done and the assessments of physical performance of Nechako River habitat complexing from 1993 to 1995.

Physical assessments were performed in the spring of each year. A video recording and visual inspection of the complexes were conducted in the fall of 1993. No new complexes were constructed from 1993 to 1995. Downstream booms were added to two railanchored sweepers and two hand-placed anchored sweepers in 1993 to improve debris capture.

Damaged or displaced complexes included:

- 3 pseudo beaver lodges;
- 7 rail-anchored sweepers;
- 8 hand-placed anchored sweepers;
- 1 pipe-pile debris catcher;
- 4 rail debris catchers; and,
- 1 pocket pool.

Of the above, the following 10 complexes were not assessed from 1993 to 1995, principally because of debris loss stemming from damage or displacement:

- 2 pseudo beaver lodges;
- 1 rail-anchored sweeper;
- 3 hand-placed anchored sweepers;
- 3 rail debris catchers; and,
- 1 pocket pool.

Fifty complexes are currently being monitored in the Nechako River.

To date, the Nechako Fisheries Conservation Program (NFCP) habitat complexing project has identified the following parameters as important for biological success in habitat complexing:

- shear velocity;
- cover area; and,
- substrate.

Additionally, it was determined that adequate complex anchoring is crucial for the maintenance of structural integrity during fluctuating flows.

The rail-anchored sweepers, hand-placed anchored sweepers, and rail debris catchers have been constructed in a manner that has maintained velocity criteria. Some early structures altered velocities such that design criteria were no longer met.

## INTRODUCTION

The Nechako Fisheries Conservation Program (NFCP) was established as a result of an agreement signed in 1987 by Alcan Aluminum Ltd., the Government of Canada, and the Province of British Columbia (Anon. 1987a). The goal of the NFCP is to ensure conservation of Nechako River chinook salmon and protection of migrating sockeye salmon. An integral component of the program is the testing and implementation of remedial measures including the modification of in-stream habitat and construction of habitat complexes.

This report documents the progress of work done on the habitat complexing project during the 1993/94, 1994/1995, and 1995/1996 program years (April 1 to March 31 of each year). All field work for this project was performed between May and October of each year. Therefore, the work is identified in this report as occurring in 1993, 1994 or 1995.

The focus of this report is on the evaluation of the physical performance of habitat complexes constructed since the inception of the project in 1988 and on the modification of these habitat complexes from 1993 to 1995. The evaluation of the biological performance of habitat complexes from 1993 to 1995 is reported elsewhere (Triton 1996a, 1996b, and 1998a).

## RATIONALE

In August 1987, a working group of technical experts from the Department of Fisheries and Oceans (DFO), Alcan, and the Province of British Columbia was established to assess how to ensure the conservation and protection of the fisheries resources of the Nechako River. The working group recognized that changes in Nechako River flows following development of the Kemano Completion Project could influence the amount of cover habitat available to juvenile chinook that use the river. This fact prompted a recommendation to increase the complexity of juvenile chinook cover habitat in the Nechako River prior to the implementation of the Long-Term Flow Regime (Anon. 1987a) to replace what cover habitat might be lost due to the flow changes in the river. A preliminary assessment of the types of habitats utilized by Nechako River chinook was conducted via snorkeling surveys in early 1988. Observations from these surveys were used to identify suitable habitat complexing designs for pilot testing. The suggested designs also benefit from the experience of NFCP Technical Committee members and from the results of previous studies on the Nechako River (Envirocon 1984a) which had developed basic habitat criteria (e.g., depth, velocity, substrate) relevant to the proposed habitat complexes.

The NFCP pilot habitat complexing project was initiated in 1988 to test these habitat complexing techniques and to assess their use by Nechako River juvenile chinook. After the 1988 pilot testing, the information on suitable designs was supplemented by a literature review of in-stream habitat complexing projects (Triton 1998b). The review indicated that, although habitat complexes had been widely used to create fish habitat, most techniques had been directed to small streams supporting fish species other than chinook. In addition, quantitative assessments of the effectiveness of these techniques were limited. A supplemental array of potential remedial measures was prepared and selected techniques appropriate to the Nechako River were pilot tested in 1989 and 1990 (Triton 1996c). Following the 1989 and 1990 tests, a short list of recommended habitat complex designs was prepared for more extensive testing. These designs were based on replicating habitat structures found naturally in the Nechako River. In 1991 pilot testing of new complexes continued, along with the replicate construction of selected complexes (Triton 1996d). In 1992 several complexes were modified (Triton 1996e). From 1993 to 1995 monitoring continued and several complexes were further modified or removed. No new habitat complexes were constructed during that period.

### **OBJECTIVES**

The objectives of the habitat complexing project are:

- to determine the hydraulic performance and durability of a variety of proposed habitat complexes through a series of small scale pilot tests;
- to continue the physical assessment of previously constructed habitat complexes; and,
- to identify cost effective methods of achieving the habitat complexing goal set out in the Nechako River Working Group Report.

## SCOPE

The scope of the NFCP habitat complexing project consisted of the following:

- Construction of a limited number of habitat complexes that have been demonstrated to work on other river systems for other species of salmon;
- (2) Construction of a limited number of habitat complexes that could duplicate naturally occurring habitat on the Nechako River;
- (3) Installation of these habitat complexes at accessible sites downstream of known spawning grounds; and,
- (4) Assessment of habitat complexes under varying flow and meteorological conditions to determine their hydraulic performance and durability.

## TYPES OF HABITAT COMPLEXES

The selection of the types of habitat complexes considered for installation in the Nechako River was based on a review of similar work on other river systems, on Nechako River conditions, and on local availability of materials. Woody debris was identified as the preferred "cover habitat" (Triton 1998b and Lister 1994). Habitat complexes identified for pilot testing in the Nechako River were of two types: structures and in-stream modifications.

- Structures consist of debris bundles and debris catchers placed along the river to provide additional cover habitat for rearing chinook juveniles. Debris bundles are trees or root masses cabled to anchors on the river bank. Debris catchers are structures placed at various locations along the stream margin to intercept and hold any large woody debris (LWD) floating downstream. These structures trap the river's natural supply of debris to provide fish habitat.
- In-stream modifications involve the excavation or placement of river bed materials to replicate existing natural morphological features found on the Nechako River.

Since 1988, 13 different habitat complex designs have been tested in the Nechako River. These designs are categorized below as either "structures" - comprised of debris bundles or debris catchers, or "in-stream modifications".

#### STRUCTURES

#### Debris Bundles

- 1) Rootwad Sweepers
- 2) Brush Piles
- 3) Floating Cribs
- 4) Pseudo Beaver Lodges
- 5) Deep Water Sweepers
- 6) Rail-anchored Sweepers
- 7) Hand-placed Anchored Sweepers

#### **Debris Catchers**

- 1) Channel Jacks
- 2) Pipe-pile Debris Catchers
- 3) Rail Debris Catchers

#### **IN-STREAM MODIFICATIONS**

- 1) Excavation of a Side Channel, complexed with debris bundles and a debris boom.
- 2) Construction of Point Bars with back eddy pools on the Nechako River shoreline.
- 3) Excavation of Pocket Pools from the Nechako River bed.

No new complexes were constructed from 1993 to 1995. Detailed descriptions of habitat complexes constructed from 1988 to 1990 are presented in Triton (1996c). Complexes constructed in 1991 and work performed in 1992 are described in Triton (1996d) and Triton (1996e). These reports detail the process and criteria for site selection and structure design, and the reader is referred to them for more information.

### SITE SELECTION AND DESIGN CRITERIA

Since 1988, the criteria used for site selection and for design of all habitat complexes have been based on a review of the general literature (Everest and Chapman 1972; Lister and Genoe 1970), and on an assessment of chinook life history data collected during field studies on the Nechako River (Envirocon Ltd. 1984a; Russell et al. 1983). Habitat complex designs were based on the Nechako River physical characteristics and natural habitats.

The selection of specific sites for habitat complexes in the mainstream Nechako River was based on criteria developed by the Department of Fisheries and Oceans (Anon. 1987b) and Envirocon Ltd. (1984b). The following criteria have been used in the site selection and design of all habitat complexes installed in the mainstem Nechako River since 1988:

Parameter	<b>Criterion Range</b>	Preferred
Velocity (m∕s)	0.15 - 0.4	0.3
Depth (m)	not less than 0.4	0.75-1.0
Substrate	gravel to cobble	gravel to cobble
Extension (m)	site specific	5.0

Note that extension is defined as the perpendicular distance from the wetted edge to the outer edge of the structure.

Habitat complexes installed in the mainstem Nechako River from 1988 through 1990 were designed to operate at the Short-Term Flow Regime spring and summer rearing flows of 56.6 m<sup>3</sup>/s (2,000 cfs), and at fall and winter flows of 31.1 m<sup>3</sup>/s (1,100 cfs) (Anon. 1987a). By comparison, complexes installed in the mainstem Nechako River in 1991 were designed to operate at expected Long-Term rearing flows of 31.1 m<sup>3</sup>/s (1,100 cfs) and were located so that they could also operate during lower water levels and river widths associated with future Long-Term winter flows of 14.2 m<sup>3</sup>/s (500 cfs). However, all complexes were only evaluated for design criteria fulfillment at approximate Nechako River high and low flows of 56.6 m<sup>3</sup>/s (2,000 cfs) and 31.1 m<sup>3</sup>/s (1,100 cfs).

The site selection and design criteria used in the construction of the side channel in the spring of 1988 were developed by DFO (Anon. 1987b) and Envirocon Ltd. (1984b) and are presented below. The construction of the side channel was such that depth and velocity at each complex in the channel would be similar to the preferred depth and velocity criteria of complexes in the mainstem Nechako River. The following criteria were developed for the side channel from the above-noted sources for approximate Nechako River high and low flows of 56.6 m<sup>3</sup>/s (2,000 cfs) and 31.1 m<sup>3</sup>/s (1,100 cfs).

Parameter Crite	<b>Criterion Range</b>				
Maximum Depth (m)	0.6				
Avg. Cross-sectionalVelocity (m/s)	approx. 0.5				
Side Channel Flow Range (m <sup>3</sup> /s)	1 - 2				
Nechako River FlowRange (m <sup>3</sup> /s)	31.1 - 56.6				

Side channel bank slopes were graded such that the right bank approximated the existing stable slope of 1.5H:1V and the left bank provided shallow habitat for newly emergent fry through a lower slope of 3.5H:1V. The side channel was assessed for the above parameters in 1996 to determine if the criteria were being achieved. Cover area was also measured during physical assessments.

It was expected that the installation of a given habitat complex would modify velocities at the site, but that the velocities throughout the complex would remain within the criteria range. Therefore, the criteria ranges apply to both the site selection and to the design of the habitat complexes.

### **PROJECT IMPLEMENTATION**

The 1993 to 1995 habitat complexing project implementation was as follows:

- Modifications were made to several existing complexes;
- Physical assessments were performed following the modifications in 1993, and in the springs of 1994 and 1995; and,
- During the fall of 1993, a video recording and visual inspection of the complexes were conducted.

Modifications to existing complexes in 1993 were based on recommendations stemming from the physical assessments and from biological sampling trips in 1992. A summary of all modifications made is presented in Table 1. Details are shown in Table A1 (Appendix A). Of the 60 structures present along the margins of the Nechako in the fall of 1992, four were modified in 1995 and ten were removed in 1993, 1994 and 1995 (four, one and five respectively). Fifty structures thus remained at the end of 1995.

In 1993, physical assessments of habitat complex performance were done during the spring (from June 5 to 10) and a video recording and visual inspection were completed in the fall, on November 19. In 1994, a physical assessment was performed in the spring from May 22 to 25, while in 1995, the assessment was performed from May 16 to 18. The assessments were general inspections of all complexes remaining in the Nechako River since the beginning of the pilot testing project in 1988. Their goals were to identify any structural damage or instability incurred over the winter period and to evaluate the achievement of design criteria. The video and visual inspection in the fall of 1993 involved an investigation of structural damage and displacement following the summer cooling flows in July and August -

Table 1           Summary of Habitat Complexing Construction Activities, 1993 to 1995													
Type of Habitat Comp	lex	Abbr.	Quantity		Quant	ity	Quantity			Ç	uantit	Quantity	
			Remaining	C	Constru	icted		Modif	ïed	R	emove	ed	Remaining
			1992	1993	1994	1995	1993	1994	1995	1993	1994	1995	1995
STRUCTURES													
Debris Bundles													
Rootwad Sweepers		RS	1	-	-	-	-	-	-	-	-	-	1
Brush Pile		BP	1	-	-	-	-	-	-	-	-	-	1
Floating Cribs		FC	2	-	-	-	-	-	-	-	-	-	2
Pseudo Beaver Lod	ges	PBL	4	-	-	-	-	-	-	-	-	2	2
Rail-anchored Swee	epers	RAS	10	-	-	-	2	-	-	1	-	-	9
Hand-placed Ancho	ored Sweepers	HAS	10	-	-	-	2	-	-	2	-	1	7
Debris Catchers													
Pipe-pile Debris Ca	tchers	PDC	2	-	-	-	-	-	-	-	-	-	2
Rail Debris Catcher	s	RDC	23	-	-	-	-	-	-	1	-	2	20
IN-STREAM MODI	FICATIONS												
Side Channel		SC	1	-	-	-	-	-	-	-	-	-	1
Side Channel Debri	s Boom	DB	1	-	-	-	-	-	-	-	-	-	1
Point Bars		PB	3	-	-	-	-	-	-	-	-	-	3
Pocket Pools		PP	2	-	-	-	-	-	-	-	1	-	1
Totals			60	0	0	0	4	0	0	4	1	5	50
Modifications: 1993	Downstream boon (LM72.9HAS, LM	ns added 175.9HA	l to improve de AS, LM82.1RA	bris car S, RM8	oture 35.7RA	S)							
Removal: 1993	Removed from assessment due to loss of debris (LM26.6RAS) Removed from assessment due to loss of loss of logs and debris (RM29.3RDC) Removed from assessment as stripped of branches by ice during winter 92/03 (LM80.0HAS, LM80.1HAS)												
1994	Removed from as	sessment	t. River bed mo	ovement	t resulte	d in loss	of compl	lex (M	C15.8PP)				
1995	Removed from ass (LM22.7RDC to c Removed from ass	Removed from assessment. River bed movement resulted in loss of complex (MC15.8PP) Removed from assessment due to loss of debris (LM22.7RDC to control, RM24.8PBL to control, RM31.0PBL to control, MC85.6RDC to natural site) Removed from assessment as stripped of branches (RM74.1HAS to natural site)											

recorded mean daily flows in Nechako River below Cheslatta Falls typically reach approximately  $283 \text{ m}^3/\text{s}$  (10,000 cfs).

Field investigations consisted of an inspection of each complex and of photographic documentation of its condition. Physical assessments of habitat complexes were conducted from shore, by boat and by snorkeling.

The following features were noted during inspections in 1993, 1994 and 1995 at each habitat complex as applicable:

- water depths and velocities upstream and downstream (at 1/3 and 2/3 of the extension), at the inside and outside shear zones, and at a flow-through point within the complex;
- cover area;
- extension from margin;
- attachment to shore;
- depth of cover;
- erosion/sedimentation;
- local substrate; damage;
- displacement; and,
- debris accumulation or loss.

Physical condition and stability were noted with reference to durability (structural integrity since the installation of the complex) and position in the river. Recommendations or comments were noted to modify or remove some complexes, and are presented in this report. This proposed work may be done in future years .

At each complex, velocity was measured with a Swoffer flow meter (model 2100) at 1/3 and 2/3 of the extension. Water depth at these locations was measured with the flow meter rod. The extension and principal cover dimensions of the complexes were measured with a survey tape. Cover areas were then calculated for each complex. The hydraulic characteristics of the complexes under various flows were documented to determine their compliance with design criteria. The amount of debris accumulation or loss was recorded to document the function of habitat complexes under prevailing Nechako River conditions. Substrate composition was noted as a relative ranking of material present. Summaries of all activities are presented in Tables 1 through 4. Construction details are presented in Table A1 (Appendix A) and the results of physical assessments are presented in Table B1 (Appendix B). Sketches and photos of the habitat complexes are presented in Appendices C and D, respectively.

#### **1993 Habitat Complex Construction Sites**

Maps of the 1993, 1994, and 1995 NFCP habitat complexing project study areas for Reaches 1, 2, and 4 including complex locations, are presented in Figures 1 and 2. The complexes were first installed in Reach 4 in 1991, when severe ice conditions were expected to test complex durability.

#### Spring 1993 Modifications to Habitat Complexes

Between April 15 and April 27, 1993, modifications were made to:

- 2 rail-anchored sweepers (LM82.1RAS, and RM85.7RAS),
- 2 hand-placed anchored sweepers (LM72.9HAS, LM75.9HAS).

The modification was to attach a tree acting as a stiffleg or downstream boom to the tip of the sweeper by a cable and to anchor the tree's other end to the shore at a point several m downstream. This design allowed the complexes to maintain their position in the current and to trap floating debris. Small diameter logs were used to permit installation of these booms by hand (due to access problems in Reach 4 and to reduce installation costs). Details of the modifications and information on site locations (km downstream from Kenney Dam) are presented in Table A1 (Appendix A).

The 1993 modifications were based on recommendations from the 1992 physical assessments of similar modifications to the pseudo beaver lodge RM24.8PBL and to the rail-anchored sweeper RM26.9RAS (Triton 1996e).

#### Spring 1993 Physical Assessment

Physical assessments of all complexes were conducted from June 5 to 10, 1993. During that period, discharge in the Nechako River ranged from 57.5 to 59.5  $m^3/s$  (2,031 to 2,101 cfs). In general, most depths were above

#### Table 2: Summary of 1993 Physical Assessment Observations

Type of Habitat Complex	Abbrev.	Quantity	Damage or	Cover Area	Cover Area	Sedimentation or	Substrate	Comments	Recommendations
		Remaining	Displacement in 1993	(m <sup>2</sup> )	Change	Erosion	(In order of		
		1993					predominance)		
STRUCTURES									
Debris Bundles									
Rootwad Sweepers	RS	1	No	65	Increased slightly from 1992	Not available	Gravel, fines	None	None
Brush Pile	BP	1	No	13	Increased slightly from 1992	No	Gravel, fines	None	None
Floating Cribs	FC	2	No	48/98	Reduced/Increased slightly from 1992	No	Gravel, fines	None	None
Pseudo Beaver Lodges	PBL	4	Frame broken in 1992 - debris lost - RM31.0PBL. Debris shifted and lost - RM31.1PBL.	7 - 50	Increased from 1992	No	Gravel, fines	Loss of debris at 2 sites, however adequate cover available in the area.	None
Rail-Anchored Sweepers	RAS	9	Broken at outer rail - RM29.4RAS. Loss of shore anchor and debris - LM26.6RAS (removed).	5 - 30	Increased from 1992	Erosion at RM16.2RAS	Gravel, cobble, fines	Two complexes failed to trap new debris. Downstream booms appeared to have helped increase cover area.	None
Hand-Placed Anchored Sweepers	HAS	8	Submerged - RM74.1HAS, Stripped of branches by ice- LM80.0HAS, LM80.1HAS (removed)	7 - 30	Increased from 1992	No	Gravel, cobble, fines	Cover area increased at 2 structures that had downstream booms added.	None
Debris Catchers									
Pipe-Pile Debris Catchers	PDC	2	Rear pile lifted by ice - RM34.7PDC. Outside piles bent on both complexes	150/180	Reduced/Increased slightly from 1992	Sedimentation downstream of larger complex (MC35.4PDC)	Gravel, fines	Complexes stable despite damage.	No
Rail Debris Catchers	RDC	22	Shore cable broken - RM16.4RDC. Loss of logs and debris - RM29.3RDC (removed)	4 - 120	Increased from 1992	Sedimentation (2)/Erosion (5)	Gravel, cobble, fines	Despite damage, most structures were stable and retained debris. Low velocities at some locations due to large cover areas and locations close to shore.	None
IN-STREAM MODIFICATIONS									
Side Channel	SC	1	No	22/27 including natural cover	Increased from 1992	Not available	Not available	Flows blocked by beaver dams since 1989, resulting in no measured velocities.	None
Side Channel Debris Boom	DB	1	No	44	Increased from 1992	Not available	Gravel, cobble, fines	Stable, despite loss of shore anchor in 1992.	None
Point Bars	РВ	3	No	Not applicable	Not applicable	Not available	Cobble, gravel	None	None
Pocket Pools	PP	2	No	Not applicable	Not applicable	Erosion at MC15.8PP	Cobble, gravel	Erosion of perimeter, cobbles and gravels deposted in MC15.8PP since 1992, making it difficult to determine boundaries	None

Type of Habitat Complex	Abbrev.	Quantity	Damage or	Cover	Cover	Sedimentation or	Substrate	Comments	Recommendations
		Remaining	Displacement in 1994	Area	Area	Erosion	(In order of predominance)		
	_	1994		(m <sup>2</sup> )	Change				
STRUCTURES									
Debris Bundles									
Rootwad Sweepers	RS	1	No	69	Similar to 1993	No	Gravel, fines, cobbles	None	None
Brush Pile	BP	1	No	37	Increased from 1993	No	Fines	None	None
Floating Cribs	FC	2	No	30/172	Reduced/Increased from 1993	No	Gravel, with fines or cobbles	Smaller crib has little debris - half of complex lifted out of water	None
Pseudo Beaver Lodges	PBL	4	No	14 - 81	Increased from 1993	No	Gravel, fines with some cobbles	Significant debris accumulation at two sites.	None
Rail-Anchored Sweepers	RAS	9	Stripped of branches - RM22.1RAS, RM26.9RAS. Broken - RM22.95RAS.	6 - 43	Increased from 1993	Increased from 1993 Sedimentation at LM82.2RAS and fines at most locations		Two complexes failed to trap new debris. Modified complexes in good condition.	New trees proposed at RM22.95RAS and RM29.4RAS.
Hand-Placed Anchored Sweepers	HAS	8	Broken tree - LM73.0HAS, Stripped of branches - RM74.1HAS, LM80.2HAS.	2 - 45	Increased from 1993	No	Cobbles, fines and gravels	Modified structures in good condition, with good debris accumulation.	New sweeper tree recommended for LM73.0HAS
Debris Catchers									
Pipe-Pile Debris Catchers	PDC	2	No	91/192	Reduced/Increased slightly from 1993	Sedimentation downstream of both complexes	Fines, gravels, cobbles	Complexes stable despite damage.	No
Rail Debris Catchers	RDC	22	No	7 - 136	Increased from 1993	Sedimentation (5)/Erosion (6)	Gravel, cobble, with boulders and fines at most locations	Despite damage, most structures were stable and provided adequate cover areas.	None
IN-STREAM MODIFICATIONS									
Side Channel	SC	1	No	32/96 including natural cover	Increased from 1993	Not available	Not available	Flows blocked by beaver dams since 1989, resulting in no measured velocities.	None
Side Channel Debris Boom	DB	1	No	32	Reduced from 1992	No	Gravel, fines, cobbles	Stable, despite loss of shore anchor in 1992.	None
Point Bars	PB	3	No	Not applicable	Not applicable	No	Cobble, fines, gravels	None	None
Pocket Pools	РР	1	Significant erosion - MC15.8PP (removed).	Not applicable	Not applicable	Continued erosion at MC15.8PP	Cobble, boulders, gravels	Erosion of perimeter, cobbles and gravels deposted in MC15.8PP since 1992, making it difficult to determine boundaries - complex removed from assessment.	None

Type of Habitat Complex	Abbrev.	Quantity	Damage or	Cover	Cover	Sedimentation or	Substrate	Comments	Recommendations
		Remaining	Displacement in 1995	Area	Area	Erosion	(In order of predominance)		
		1995		(m <sup>2</sup> )	Change		_		
STRUCTURES									
Debris Bundles									
Rootwad Sweepers	RS	1	No	55	Reduced from 1994	Sedimentation	Fines and gravel	None	None
Brush Pile	BP	1	No	4	Reduced from 1994	No	Fines and gravel	Movement of river bank resulted in dewatering of the complex.	None
Floating Cribs	FC	2	No	23/91	Reduced from 1994	No	Fines and gravel	Smaller crib has little debris trapped.	None
Pseudo Beaver Lodges	PBL	2	Two removed due to loss of debris - RM24.8PBL, RM31.0PBL.	21/50	Similar to 1994	No	Gravels and fines	None	None
Rail-Anchored Sweepers	RAS	9	Three broken - RM22.1RAS near outside anchor, LM29.4RAS outside anchor lost, LM82.2RAS anchor stump broken. Reduced to bare log - RM22.95RAS. Stripped of branches - RM16.2RAS.	1 - 24	Reduced from 1994	Sedimentation at LM82.2RAS	Gravel and cobble, with boulders or fines at most complexes.	None	None
Hand-Placed Anchored Sweepers	HAS	7	Displaced - LM32.65HAS. Reduced to bare log - LM72.9HAS, LM73.0HAS, LM78.0HAS. Removed - RM74.1.	2 - 15	Reduced from 1994	Sedimentation at 2 sites.	Gravel, fines, cobbles	None	None
Debris Catchers									
Pipe-Pile Debris Catchers	PDC	2	Downstream pile broken - RM34.7PDC.	42/149	Reduced from 1994	Sedimentation downstream of larger complex	Fines and gravel	Smaller complex lost debris due to loss of pile.	No
Rail Debris Catchers	RDC	20	Two removed due to loss of debris - LM22.7RDC and MC85.6RDC.	8 - 137	Similar to 1994.	Sedimentation (3)/Erosion (11)	Gravel, cobble and fines at most locations	None	None
IN-STREAM MODIFICATIONS									
Side Channel	SC	1	No	Not available	Not applicable	Not available	Gravel, fines and cobbles.	Flows blocked by beaver dams since 1989, resulting in no measured velocities.	
Side Channel Debris Boom	DB	1	No	60	Increased from 1994	Some sedimentation downstream of complex.	Fines, gravel and cobbles	Stable, despite loss of shore anchor in 1992.	None
Point Bars	PB	3	No	Not applicable	Not applicable	No	Cobbles, gravel and fines	None	None
Pocket Pools	PP	1	No	Not applicable	Not applicable	Not available	Cobble, boulders and gravel	None	None





the minimum criterion limit of 0.4 m. Overall, 1/3 of the velocities were distributed within the criterion range of 0.15 to 0.40 m/s, 1/3 below and 1/3 above it. Upstream velocities were generally within the criterion range, while flow-through and downstream velocities were generally below that range. Outside and inside shear velocities were generally above the range. Observations from those assessments and recommendations are summarized below and in Table 2. Details are presented in Table B1 (Appendix B).

#### **Structures**

#### <u>Debris Bundles</u>

In 1993, the majority of debris bundles were stable with cover areas generally greater than those measured in 1992. Gravel was the predominant substrate, with fines or cobble also present.

Damage or displacements were noted for two pseudo beaver lodges, two rail anchor sweepers, and three hand placed anchored sweepers. Three structures were removed. Details are as follows:

- The frame on pseudo beaver lodge RM31.0PBL was broken in 1992. As a result, the accumulated debris shifted and was lost from the complex structure.
- Rail-anchored sweeper LM26.6RAS was removed after the loss of its shore anchor and debris. An outer rail broke at rail-anchored sweeper RM29.4RAS.
- Hand-anchored sweepers LM80.0HAS and LM80.1HAS were stripped of branches by ice, and both structures were removed. Complex RM74.1HAS was submerged due to high flows.

#### <u>Debris Catchers</u>

The two pipe-pile debris catchers continued to maintain very large cover areas of 150 and 180 m<sup>2</sup>. The rear pile of the smaller complex had been lifted from the river bed by ice and was near failure. The outside piles were bent on both complexes. Despite the damage, the complexes were stable. Sedimentation was apparent downstream of the larger complex, due to large cover areas and low velocities.

One rail debris catcher (RM29.3RDC) was removed from the 1993 assessment due to the loss of its logs and de-

bris during the 1992 summer cooling flows. Structure RM16.4RDC had its shore cable broken, resulting in a loss of debris. Debris accumulation was observed at several complexes, and cover area of the 22 rail debris catchers had increased, ranging from 4 to 120 m<sup>2</sup>. Gravel was the predominant substrate, with cobbles and fines present at the majority of the complexes. Erosion was observed at five of the complexes, and sedimentation occurred behind the complexes at two sites. Large cover areas and positioning in the river resulted in low velocities through some of the complexes, with flow passing outside them.

#### In-Stream Modifications

No new damage or displacement were noted on the instream modifications in 1993. However, low or near zero velocities were observed in the side channel that became blocked in 1991.

The area of the debris trapped by the boom at the upper end of the channel increased to  $44 \text{ m}^2$  and additional debris was observed on the shore. The complex was stable despite the shore deadman anchor having been unearthed in 1992, and no further displacement had occurred.

No damage to the point bars was visible during the spring physical assessment. Cobble and gravel were the dominant substrates.

The pocket pool located in the high velocity area (MC15.8PP) continued to erode along its perimeter. Cobbles and gravels had been deposited within the pool, making it very difficult to locate the complex and determine its boundaries.

#### Fall 1993 Physical Assessment

On November 19, 1993, a visual inspection and video recording of the habitat complexes were to complete any damage or displacement following summer cooling flows in July and August. The inspection showed that two rail-anchored sweepers were broken in half, yet their cover areas remained similar to their spring values. Information on the fall assessment is presented in Table B2 (Appendix B).

#### **Spring 1994 Physical Assessment**

All complexes were assessed from May 22 to 25, 1994. The discharge in the Nechako River below Cheslatta Falls was similar to that of spring 1993, ranging from 56.7 - 57.5 m<sup>3</sup>/s (2,002 to 2,031 cfs). Most depths measured were above the minimum criterion limit of 0.4 m. As in 1993, about 1/3 of the velocity measurements were within the criterion range of 0.15 to 0.40 m/s, 1/3 were below and 1/3 were above it. Upstream velocities measured at 1/3 extension were generally below the criterion, while upstream velocities at 2/3 extension were generally above it. Outside and inside shear velocities were generally above the criterion. Flow-through velocities were usually either within or below the criterion, while downstream velocities were generally below it. The observations from the assessments are summarized below and in Table 3. Details are presented in Table B3 (Appendix B).

#### **Structures**

#### <u>Debris Bundles</u>

In 1994, the majority of debris bundles were stable, with cover areas generally increased from 1993. The following damages was noted:

- Rail-anchored sweepers RM22.1RAS and RM26.9RAS were stripped of their branches and the tree at RM22.95RAS was broken.
- Similarly, hand-placed anchored sweepers RM74.1HAS and LM80.2HAS were stripped of their branches and the tree at LM73.0HAS was broken.

#### <u>Debris Catchers</u>

As in 1993, the two pipe-pile debris catchers maintained very large cover areas of about 91 and 192 m<sup>2</sup>. The complexes were stable despite some damage to the pilings. Sedimentation was observed again downstream of both complexes.

The rail debris catchers were generally stable and provided increased cover areas over 1993, ranging from 7 to 136 m<sup>2</sup>. Erosion was observed at six complexes, and sediment accumulations were found behind five complexes.

#### In-Stream Modifications

Low water velocities in the side channel were again observed in 1994. The cover area of the debris bundles within the side channel was estimated at  $32 \text{ m}^2$ . However, the cover area increased to about 96 m<sup>2</sup> when natural cover was included.

The debris boom's cover area was relatively stable at  $32 \text{ m}^2$ . The structure continued to be in good condition, with no displacement even with its shore deadman damaged.

The point bars continued to be in good condition in 1994, with no damage or displacement noted.

Due to significant erosion of the pocket pool in the high velocity location, this complex was not assessed in the spring of 1994. In 1994, the remaining lower velocity complex had an area of 49  $m^2$ . The substrate consisted mainly of cobbles and boulders, with no erosion or sedimentation noted.

#### **Spring 1995 Physical Assessment**

All complexes were assessed from May 16 to 18, 1995. The discharge at the Nechako River below Cheslatta Falls was higher than in 1993 or 1995 at 62.3  $m^3/s$  (2,200 cfs). Most depths measured were again above the minimum criterion limit of 0.4 m. As in 1993, about 1/3 of the velocity measurements were within the criterion range of 0.15 to 0.40 m/s, 1/3 were below and 1/3 were above it. Upstream velocities at 1/3 extension were generally below or within the criterion, while upstream velocities at 2/3 extension were generally above it. Outside shear velocities were generally above the criterion while inside shear velocities were generally within it. Flow-through velocities were usually below the criterion and downstream velocities were generally below it. The observations from the assessments are summarized below and in Table 4. Details are shown in Table B4 (Appendix B).

#### **Structures**

#### <u>Debris Bundles</u>

In 1995 the debris bundles were generally stable, but cover areas were generally reduced from 1994. Damage or displacements were observed as follows:

- Two pseudo beaver lodges (RM24.8PBL and RM31.0PBL) had lost all debris and were therefore removed.
- Three rail-anchored sweepers were damaged - the tree at RM22.1RAS was broken near its outside anchor, LM29.4RAS had lost its outside anchor and LM82.2RAS had its anchor stump broken.
- Rail-anchored sweepers RM16.2RAS and RM22.95RAS were stripped of branches.
- The hand-placed anchored sweeper LM32.65HAS was displaced to shore, and LM72.9HAS, LM73.0HAS, LM78.0HAS were reduced to bare logs. The complex RM74.1HAS was removed from further assessment as it had been completely defoliated since 1993.

#### <u>Debris Catchers</u>

The cover areas of the two pipe-pile debris catchers were smaller than in 1994, having been reduced from 91 and  $192 \text{ m}^2$  to 42 and 149 m<sup>2</sup>. The smaller complex lost a significant amount of debris as its downstream pile finally broke after several years of uplift and loosening during winter. No displacement was observed to the other complex although sediment continued to accumulate immediately downstream of the structure. The substrate generally consisted of fines and gravel. No recommendations were made for any repairs.

In 1995, two rail debris catchers were subsequently removed from ?? biological and physical assessments due to loss of debris after the summer cooling flows in 1994. Complex LM22.7RDC was changed to a control site and complex MC85.6RDC was changed to a natural site. The remaining rail debris catchers were generally stable with cover areas ranging from 8 to 137 m<sup>2</sup>. Gravel was the predominant substrate, with cobbles and fines also generally present. Erosion was observed at 11 of the complexes, and sediment accumulation at three complexes.

#### In-Stream Modifications

In 1995, a beaver dam blocking the flows in the side channel resulted in near zero velocities in the channel. Cover area of the debris bundles or natural debris was not recorded in 1995. Gravel and fines were the dominant substrates. Cover area of the debris boom increased from 1994 to about  $60 \text{ m}^2$ . The structure remained stable despite damage to its shore deadman. Fines and gravels were the dominant substrates, with cobbles also present. Some sedimentation was observed downstream of the complex.

No damage or displacement were noted for the point bars. Cobbles were the dominant substrate.

No damage nor erosion nor sedimentation were noted on the remaining pocket pools. The substrate consisted mainly of cobbles and boulders.

#### **Construction Methods**

Modifications made to existing habitat complexes in 1993 were completed manually with chain saws, power drills and oxyacetylene cutting torches. A work boat with a jet-converted outboard motor was used for the transport of personnel and miscellaneous materials. Locally available materials used in the modification of complexes included available LWD, and timber such as pine and spruce. Materials transported to the sites included cables, clamps and anchor material. Cables were secured to anchors and/or LWD by threading and looping the cables through holes in the timber, and then attaching the two ends together with cable clamps.

#### **Construction Costs**

Approximately \$4,400 were spent on the modification of habitat complexes in 1993 (Table 5). The total cost was based on an estimated unit cost of \$1,100 (\$600 in fees and \$500 in disbursements) to add downstream booms to two rail and two hand-placed anchored sweepers. The estimated costs include all charges associated with labour, materials, equipment, and other disbursements.

## OBSERVATIONS ON HABITAT COMPLEX PERFORMANCE

The evaluation of the structural performance of some complexes is still at an early stage. It is also early to judge the long-term durability of items used in the anchoring of complexes (cable, chain, clamps) as these items may corrode in the future. However, it is instruc-

Summary of I	Habitat Co	Table 5 mplexing (	Construc	ction Costs in 1993*
Type of Habitat Complex	Quantity Modified (Units)	Cost (\$/Unit)**	Total Cost	Comments
Rail-anchored Sweeper	2	\$1,100	\$2,200	Addition of downstream boom to improve debris capture.
Hand-placed Anchored Sweeper	2	\$1,100	\$2,200	Addition of downstream boom to improve debris capture.
Total Construction Cost - 1	993		\$4,400	
* Costs presented are	estimates fo	or the modifi	cation of	existing structures only. No

\* Costs presented are estimates for the modification of existing structures only. No new complexes were constructed in 1993.

\*\* Cost estimates based on \$600 in fees and \$500 in disbursements for reach unit, excluding GST.

tive to examine the performance of the habitat complexes constructed to date to develop some understanding of the factors affecting complex durability and/or performance. These observations can be used to further evaluate the criteria used in the design and siting of the complexes. This section summarizes the condition of complexes since their construction and factors affecting their biological and physical performance.

#### Structures

#### Debris Bundles

#### <u>Rootwad Sweepers</u>

The last remaining rootwad sweeper of the original four complexes constructed in 1988 was modified in 1990 to reduce seeded material. The other three structures were removed due to the failure of the stapling of cable anchors. The last complex has remained stable, with no damage or displacement noted. This is most likely a result of its location in a low velocity, shallow area. No modifications to this complex were recommended as it has performed satisfactorily.

#### <u>Brush Pile</u>

The brush pile complex installed in 1988 has remained stable. However, its cover area has fluctuated from as high as 37 m<sup>2</sup> in the spring of 1991 to as low as 4 m<sup>2</sup> in the spring of 1995 due to changes in shoreline associated with changes in water levels. Some sedimentation

was observed in the fall of 1992 and fines have been the dominant substrate in recent years. No modifications were recommended to this complex from 1993 to 1995. The small sample size (1) limits the conclusion that can be made about stability, design, performance and durability of this type of complex.

#### <u>Floating Cribs</u>

The two floating cribs installed in 1988 have generally provided significant amounts of cover. In 1991, the smaller complex was moved further into the current in an effort to increase velocities. Anchoring was improved

by securing the complex to two steel rails driven into the river bed. However, this complex was displaced onto the shore and its downstream stiff-leg was broken in 1992. The upstream floating crib was colonized by beavers in the fall of 1989 and has been left untouched since. In recent years, the cover areas of these complexes have been reduced, with the smaller complex not providing as much cover as it is partially dewatered and because its woody debris extend over only part of the structure. Both floating cribs have generally been stable, with no damage or displacement noted since 1993.

#### <u>Pseudo Beaver Lodges</u>

The design of the pseudo beaver lodges was modified in the fall of 1989 to better maintain position in the river following flow recession. However three modified units continued to lose debris in 1991. An extra boom was added to one complex prior to reseeding to provide additional flotation and to assist in debris retention in the spring of 1992. This modification appeared to help retain debris over the summer cooling flows. However, this complex and two others were again damaged or displaced at higher flows. The cover areas of these complexes were therefore significantly reduced at most sites. In 1995, due to continued debris loss, two pseudo beaver lodges (including the structure modified in 1992) were removed from further biological and physical assessments.

#### Rail- Anchored Sweepers

During the summer of 1991, 10 rail-anchored sweepers were installed along the Nechako River. Three sweepers were modified in 1992 as a result of damage incurred during the 1991 and 1992 summer cooling flows. In 1993, two sweepers were modified with the addition of downstream tree booms to improve debris capture. One of the rail-anchored sweepers was removed after having been repaired in 1992, as it had lost its shore anchor for the second time and lost much debris.

Between 1993 and 1995, most of the nine sweepers were damaged, either at the trees or at the anchor points. Several of the sweepers were stripped to the point of being reduced to bare logs.

As reported in Triton (1996e) the rail-anchored sweepers have required significant repairs during their rather short lives in the Nechako River. The short rails installed on these complexes allow little vertical movement of the sweepers as water levels rise, which may account for the lack of collected debris. They also become submerged at higher flows and lose accumulated debris. Additionally, the single tree which serves to collect debris is susceptible to loss of its branches due to stripping and to damage under larger flows.

The downstream booms added to two complexes in 1993 initially increased debris entrapment and helped to reduce the loss of cover area over time. However, these structures were significantly reduced in size between 1993 and 1995. Only smaller logs could be used as these additional booms were placed by hand. The small booms were not very effective as they became submerged at high flow under the debris load.

#### Hand-Placed Anchored Sweepers

In 1991, a total of 11 hand-placed anchored sweepers were installed - two in Reach 2 and nine in Reach 4, where there is no heavy equipment access. One of these complexes was displaced in Reach 2 during the 1991 summer cooling flows and omitted from further physical assessment. A second displaced complex in Reach 2 was repaired in the spring of 1992, only to fail again during that summer's cooling flows. Two hand-placed anchored sweepers in the spring of 1993, and another one in 1995, were removed from biological and physical assessments in Reach 4 due to loss of branches reducing their cover area. As with rail-anchored sweepers, these complexes were not successful in capturing additional debris, and tended to be stripped, damaged or displaced during winter ice movement and high summer flows. Hand-placed anchored sweepers suffer from problems similar to the railanchored sweepers, i.e. lack of stability under increased flows and stripping of branches. Downstream booms added to two complexes in 1993 did not prevent one unit from being stripped to the point of turning into a bare log. The second modified unit was significantly reduced in size between 1993 and 1995. As noted above, boom placement by hand does not allow large enough logs to be used.

#### **Debris Catchers**

#### Pipe-Pile Debris Catchers

Since their installation in 1989, the two pipe-pile debris catchers have been generally stable under variable flow conditions, despite both complexes pilings being bent or pulled from the river bed. Sedimentation was observed at both sites from 1993 to 1995, due to the large size of the complexes and low velocities. In 1995, the smaller complex lost a significant amount of debris following the loss of its downstream piling. No recommendations were made for any repairs as the structures are still intact and maintain large cover areas.

#### Rail Debris Catchers

Seven large-sized rail debris catchers were constructed in 1990. In 1991, an additional 16 smaller catchers were constructed to maintain more manageable debris piles. The first large rail debris catchers have been generally quite durable. However, the smaller structures have required regular repairs and reseeding following summer cooling flows.

From 1993 to 1995, three rail debris catchers (two built in 1991 and one built in 1990) were removed from the assessment due to loss of logs and debris following summer cooling flows. Despite structural damage in 1992, most remaining complexes were stable and maintained cover areas of up to 137 m<sup>2</sup>. Triton (1996e) suggested that the repeated damage to the newer complexes may be partially due to the down-scaling of complex size in 1991.

To match the durability of the older complexes, the log boom diameter of future complexes may have to be increased to prevent breakage at the anchor points. Stronger cable anchoring should also be considered. In addition, the attachment of the chains connecting the booms to the rails should be redesigned to prevent loss of accumulated debris and loss of boom logs over the rails during high summer flows. The chains could be directly attached to eyes in the rails with sufficient slack to allow the logs to rise and fall with changes in water level. Finally, the aesthetics of these structures have been an issue since their construction. Methods to camouflage the steel components are being investigated.

#### **In-Stream Modifications**

#### Side Channel

The original side channel with full spanning complexes and a debris boom built in 1988 had problems with excessive debris accumulation. As a result, in 1990, the debris boom was moved upstream of the channel entrance to prevent excessive loading within the channel. In addition, the full spanning habitat complexes in the side channel were removed and replaced with smaller single logs buried at intervals along the margins (Triton 1996c). Despite these modifications, low flows and subsequent construction of dams by beavers within the side channel resulted in velocities well below criteria limits. From 1993 to 1995, flows in the side channel continued to be blocked and velocities measured zero. No recommendations for improvements have been made as lack of adequate flow and continual beaver dam blockage has made the complex undesirable for long term use.

The debris boom installed upstream of the side channel in 1990 was designed to prevent excessive debris accumulation in the side channel. Although the shore deadman anchor was unearthed in 1992, the complex has remained stable, and no further displacement has occurred. The complex has been successful in trapping and retaining debris and has increased in size to approximately 60 m<sup>2</sup> in 1995. No specific recommendations were made; because of the damage incurred, however, the complex should be monitored for displacement during subsequent visits.

#### <u>Point Bars</u>

The point bars were modified in 1991 to reduce their extension and to increase their elevation. This was done to encourage formation of a back eddy and to reduce erosion of the surface during overtopping of the complexes during high summer flows. There has been no damage to the complexes since these modifications. Fines were deposited in the back eddy pools of these complexes in 1992, indicating that downstream velocities were low.

#### <u>Pocket Pools</u>

The two pocket pools constructed during the summer of 1991 were subject to either low velocities and sedimentation, or high velocities and channel scouring, depending on the location. In 1992, deposition of fines was apparent within the low velocity pool, while significant erosion of the high velocity pool's sides had taken place, making it difficult to locate and determine its boundaries.

In 1994, due to significant erosion of the high velocity pocket pool, this complex was removed from further assessment. The remaining lower velocity complex continues to provide an adequate pool area with no noted erosion or sedimentation.

#### **Resistance to Winter Physical Conditions**

During 1991, complexes were installed in Reach 4 of the Nechako River in an effort to expose the complexes to more severe ice conditions. These complexes were assessed for winter resistance for the first time in 1992.

From 1993 to 1995, several rail-anchored sweepers and hand-placed anchored sweepers lost branches or were damaged. In 1993, two hand-placed anchored sweepers located in high velocity areas of Reach 4 were severely damaged by ice and were removed from biological and physical assessments. Rail-anchored sweepers located in Reach 2 also experienced some damage.

In addition, both pipe-pile debris catchers in Reach 2 have had their pilings lifted from the river bed by ice. Rails used in the construction of other habitat complexes have also been uplifted. If this trend continues, these structures may suffer the same problems as RM34.7PDC, and lose much or all of their debris.

As some sites in Reach 4 experience higher velocities and stage changes than in Reach 2, damage to structures in Reach 4 may also occur during the summer cooling flows. It should be noted that in addition to more severe ice and high flow conditions, Reach 4 also experiences lower debris recruitment which limits the size of its structures compared to those of Reach 2.

#### **Factors Affecting Biological Performance**

Visual observations confirm that the man made habitat structures are well used by juvenile chinook salmon during the spring rearing period. Large schools of chinook are often seen in the debris and the shear zones of various structures during the biological assessments (Triton 1996a, b, f, and g, and 1998a). Electrofishing results have shown that the man made structures are also used by overwintering chinook juveniles.

The physical factors affecting the observed density of chinook juveniles in habitat complexes during snorkel surveys have been analyzed since 1991 (Triton 1996a, b, f, and g, and 1998a). Cover area is usually positively correlated with chinook abundance. Other important variables include shear velocity and substrate. Chinook abundance is negatively correlated with fines (Triton 1996f), and complexes should therefore be located in areas of gravel and cobble substrate. These should provide sufficient velocity to maintain adequate flowthrough to minimize deposition of fines.

Site selection is essential in establishing a complex which fulfills velocity design criteria over the full range of flows. The target species of fish will also influence the cover area design range and the type of complex . In the case of chinook salmon, habitat complexes which impede velocities should be avoided, and should have the appropriate cover density.

Since the beginning of this project, the rail-anchored sweepers, hand-placed anchored sweepers, and rail debris catchers have generally provided acceptable velocities and cover areas. These designs could be improved to also provide long term durability.

#### **Factors Affecting Physical Performance**

Anchoring systems for habitat complexes must be secured adequately. The deadman and rail anchoring systems used in the NFCP habitat complexing project have been successful. The suggested method of attaching cable to anchors and LWD is the looping and threading method. Stapling of cable has proved to be unsuccessful. Anchoring systems must also be designed to function under variable and transient flow conditions. The adaptability of habitat complex anchoring systems to changing flow conditions and site-specific conditions is particularly important for maintaining position and stability following flow recession. Successful complexes move with fluctuating flows so that the structures do not become submerged during high flows. Stripping or other damage to the structure is therefore less likely, and accumulated debris do not drift out of the complex.

### SUMMARY AND RECOMMENDATIONS

Since 1988, the NFCP pilot habitat complexing program has constructed and tested 13 different complex designs.

No new complexes were constructed from 1993 to 1995. Downstream booms were added to two rail-anchored sweepers and two hand-placed anchored sweepers in 1993 to improve debris capture.

Damaged or displaced complexes included:

- 3 pseudo beaver lodges;
- 7 rail-anchored sweepers;
- 8 hand-placed anchored sweepers;
- 1 pipe-pile debris catcher;
- 4 rail debris catchers; and,
- 1 pocket pool.

Of the above, the following 10 complexes were removed from assessment from 1993 to 1995, principally due to debris loss stemming from damage or displacement:

- 2 pseudo beaver lodges;
- 1 rail-anchored sweeper;
- 3 hand-placed anchored sweepers;
- 3 rail debris catchers; and,
- 1 pocket pool.

Fifty complexes are currently being monitored in the Nechako River.

To date, the NFCP habitat complexing project has identified the following parameters as important for biological success in habitat complexing:

- shear velocity;
- cover area; and,
- substrate.

Additionally, it has been determined that adequate complex anchoring is crucial for the maintenance of structural integrity during fluctuating flows. The rail-anchored sweepers, hand-placed anchored sweepers, and rail debris catchers have generally provided acceptable velocities and cover areas.

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Appendix A

1993 to 1995 Summary of Habitat Complexing Modification and/or Removal Rationale

#### Appendix A 1993 to 1995 Summary of Habitat Complexing Modification and/or Removal Rationale

Location	Site	93	93	94	94	95	95	Nature of Modification	Modification and/or Removal Rationale
(km)	Number	Sp	Fa	Sp	Su	Sp	Su		
Reach 2									
15.6	LM15.6RAS								
15.0	MC15 7PP								
15.8	MC15.8PP			R				Removed from assessment (94Sn)	River bed movement resulted in loss of complex
16.2	RM162RAS							Removed nom assessment (7 top).	
16.5	RM16 5RDC								
16.8	RM16 8RDC								
17.0	RM17 0PB								
17.15	RM17 15PB								
17.13	RM17 3PB								
17.9	RM17.9DB								
17.9-18.6	RM17.9SC								
18.3	LM18 3RDC								
20.65	RM20 65RDC								
20.05	I M21 3RDC								
21.5	LM214RDC								
22.0	RM22 ORDC								
22.0	RM22 1RAS								
22.1	RM22 55RDC								
22.55	LM22.68DC								
22.0	Linzz.onDe								Lost almost all debris. Maintained as a control
22.7	LM22 7RDC					R		Removed from assessment (95Sn)	site
22.85	LM22 85RDC							reme ee nom assessment (sesp).	
22.95	RM22.95RAS								
23.0	RM23.0RDC								
24.2	LM24.2RDC								
24.3	LM24.3RDC								
24.35	RM24.35RS								
24.4	RM24.4FC								
24.6	RM24.6PBL								
									Lost almost all debris. Maintained as a control
24.8	RM24.8PBL					R		Removed from assessment (95Sp).	site.
25.4	RM25.4RDC								
25.7	MC25.7RDC								
									Onshore anchor pulled second time. Lost all
26.6	LM26.6RAS	R						Removed from assessment (93Sp).	debris in summer 1992.
26.9	RM26.9RAS								
27.4	RM27.4FC								
28.4	RM28.4RDC								
29.4	LM29.4RAS								
									Lost logs over rails in summer 1992 and lost all
29.3	RM29.3RDC	R						Removed from assessment (93Sp).	debris.
									Lost almost all debris. Maintained as a control
31.0	RM31.0PBL					R		Removed from assessment (95Sp).	site.
31.1	RM31.1PBL								
31.4	RM31.4BP								
32.65	LM32.65HAS								
34.7	RM34.7PDC								
35.4	MC35.4PDC								

#### Appendix A (continued) 1993 to 1995 Summary of Habitat Complexing Modification and/or Removal Rationale

Location	Site	93	93	94	94	95	95	Nature of Modification	Modification and/or Removal Rationale
(km)	Number	Sp	Fa	Sp	Su	Sp	Su		
Reach 4									
72.9	LM72.9HA	S M						Addition of downstream boom.	To improve debris capture.
73.0	LM73.0HA	S							
									Completely stripped of branches, just bare log
74.1	RM74.1HA	S				R		Removed from assessment (95Sp).	remaining. Maintained as a natural site.
75.9	LM75.9HA	S M						Addition of downstream boom.	To improve debris capture.
78.0	LM78.0HA	S							
80.0	LM80.0HA	S R						Removed from assessment (93Sp).	Branches stripped by ice during winter 92/93
80.1	LM80.1HA	S R						Removed from assessment (93Sp).	Branches stripped by ice during winter 92/93
80.2	LM80.2HA	S							
80.9	LM80.9RD	2							
82.1	LM82.1RA	S M						Addition of downstream boom.	To improve debris capture.
82.2	LM82.2RA	S							
82.3	LM82.3HA	S							
83.0	LM83.0RD0	Ĵ							
05.6	MC05 (DD	~				р			Lost almost all debris. Maintained as a natural
85.6	MC85.6RD	C				ĸ		Removed from assessment (958p).	site.
057	DM05 7D A	C M							Old sweeper removed by ice in winter 92/93. D/s
85.7	RM85./RA	S M						Replaced sweeper and added d/s boom.	boom added to improve debris capture
86.35	RM86.35RD								
80.375	KW160.373K1	<i>i</i>							
	Where	$\mathbf{RS} = \mathbf{r}$	ootw	ad sv	veene	-r		Sp = Spring	
	where,	BP = h	rush	nile	eept			$S_{P} = S_{P}$	
		FC = f	loatii	19 cri	b				
		PBL =	pseu	do be	eaver	r lods	e e	$\mathbf{M} = \mathbf{modified}$	
		RAS =	rail-	anch	ored	swee	eper	$\mathbf{R} = \mathbf{removed}$	
		HAS =	han	d-pla	ced a	ancho	ored s	weeper	
		CJ = cl	hann	el iac	k				
		PDC =	pipe	-pile	debi	ris ca	tcher		
		RDC =	rail:	debri	is cat	tcher			
		SC= si	de cl	nanne	el l				
		DB = c	lebri	s boo	m				
		PB = p	oint	bar					
		PP = p	ocke	t poo	1				
		r		•					

Appendix B

1993 to 1995 Physical Assessments of Habitat Complexes

Substrate B C G F				
Erosion/Sedimentation	N/A N/A N/A N/A No N/A N/A N/A	Little erosion NA NA NA NA NA NA NA NA NA NA NA NA	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	No No No No No NA NA NA NA NA Errston/Jenostition of sediment/cravel behind commet
Cover to	Yes NVA NVA NVA Yes Yes NVA NVA NVA NVA	1 7 7 7 8 7 7 8 7 8 7 8 7 8 7 8 7 8 7 8	Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes	Yes Yes Yes Yes Yes Yes Yes Ves
Attached to Shore?	Yes N/A N/A N/A No No Yes Yes Yes	res No Yes Yes Yes Yes Yes Yes Yes	Y es Y es Y es Y es Y es Y es Y es Y es	Yes Yes Yes Yes No Yes Yes Yes
Ext. from Margin (m)	8.0 N/A N/A N/A N/A N/A 7.5 7.0 7.0 7.0 7.0 7.0 6.0	9.0 8.0 16.5 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	8.0 9.5 16.0 10.0 7.0 7.0 7.0 8.0 8.0 8.0 8.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5	7.0 3.5 8.0 8.0 7.0 7.0 8.0 6.0 6.0 7.0
Cover Area (m <sup>2</sup> )	00074000;	27 27 27 20 50 50 50 50 50 50 50 50 50 50 50 50 50	30 120 55 55 55 55 55 55 56 57 14 25 56 57 13 13 13 13 13 13 13 13 13 13 13 13 13	21 9 9 9 9 9 30 8 13 8 8
d/s 2/3 ext (m/s)	0.00	0.17 0.05 0.00 0.00 0.00 0.00 0.07 0.07 0.07 0.07 0.07 0.07 0.023	$\begin{array}{c} 0.18\\ 0.15\\ 0.14\\ 0.03\\ 0.04\\ 0.00\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.00\\ 0.00\\ 0.00\\ 0.03\\ 0.00\\ 0.00\\ 0.03\\ 0.00\\$	0.18 0.27 0.00 0.11 0.18 0.18 0.16 0.10 0.10 0.18 0.18 0.18
d/s 1/3 ext. (m/s)	0.08 0.26 0.67 0.19 0.19 0.10 0.10	0.00 - 0.00 0.17 0.58 0.00 0.00 0.00 0.00 0.19 0.19 0.23	0,13 0,07 0,07 0,07 0,09 0,09 0,09 0,09 0,09	0.30 0.07 0.04 0.04 0.13 0.06 0.14 0.14 0.14 0.14 0.10 0.33
Through (m/s)	0.38 0.44 0.16 0.35 	0.32 0.00 0.00 0.00 0.19 0.19 0.13 0.14 0.13 0.13 0.13 0.22 0.29 0.20 0.20 0.20 0.22 0.23	$\begin{array}{c} 0.09\\ 0.03\\ 0.03\\ 0.19\\ 0.03\\ 0.01\\ 0.02\\ 0.02\\ 0.01\\ 0.01\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.02\\ 0.00\\ 0.02\\ 0.00\\ 0.00\\ 0.02\\ 0.00\\$	0.31 0.11 0.09 0.13 0.13 0.13 0.10 0.10 0.10 0.10
Velocity Inside Shear (m/s)	0.26 0.26 0.62 0.49 N/A	N/A - N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	NNA NNA NNA NNA NNA NNA NNA NNA NNA NNA	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
Outside Shear (m/s)	0.59 0.12 0.60 1.09 0.63 0.63 0.75 0.75 0.74	0.50 0.66 0.87 0.80 0.80 0.80 0.53 0.53 0.63 0.53 0.53	1.1.6 0.87 0.34 0.35 0.67 0.67 0.73 0.68 0.91 0.91 0.91 0.91 0.91 0.61 0.61 0.61 0.61 0.61	0.67 0.92 0.24 0.69 0.62 0.62 0.62 0.61 1.11 1.11 0.41 1.43 0.71 0.71
/s 2/3 ext. (m/s)	0.45 - 0.69 0.23 0.47 -	0.13 0.10 0.50 0.50 0.42 0.52 0.26 0.23 0.23 0.23 0.23 0.23 0.22 0.37 0.54 0.50 0.52 0.23 0.22 0.52 0.23 0.52 0.23 0.22 0.52 0.26 0.54	0.31 0.60 0.35 0.35 0.35 0.24 0.29 0.29 0.35 0.29 0.35 0.29 0.23 0.23 0.23 0.23 0.23 0.23	$\begin{array}{c} 0.10\\ 0.11\\ 0.55\\ 0.55\\ 0.37\\ 0.36\\ 0.36\\ 0.48\\ 0.61\\ 0.47\\ 0.47\\ 0.47\\ 0.62\\ 0.62\\ 0.62\\ 0.63\\ 0.63\end{array}$
u/s 1/3 ext. u (m/s)	0.14 0.23 0.52 0.39 0.11 0.11	0.11 - 0.34 0.11 0.36 0.29 0.18 0.29 0.00 0.00 0.00 0.15 0.15	$\begin{array}{c} 0.17\\ 0.19\\ 0.19\\ 0.19\\ 0.19\\ 0.22\\ 0.22\\ 0.26\\ 0.23\\ 0.23\\ 0.26\\ 0.22\\ 0.03\\ 0.01\\ 0.11\\ 0.12\\ 0.10\\ 0.10\\ 0.12\\ 0.24\\$	0.00 0.18 0.19 0.09 0.00 0.04 0.14 0.18 0.18 0.28 0.28 0.28 0.32
l/s 2/3 ext. (m)	0.42	0.27 - 0.70 0.92 0.92 0.67 0.67 0.67 0.67 0.67 0.85 0.90	0.90 0.95 0.65 0.65 0.65 0.65 0.65 0.68 0.88 0.88 0.89 0.93 0.93 0.93 0.93 0.93 0.93 0.93	0.95 0.54 0.54 0.84 0.75 0.81 0.81 0.81 0.81 0.81 0.96 0.55 1.30
d/s 1/3 ext. 6 (m)	0.20 0.17 0.35 0.36 0.40 0.40 0.55	0.20 - 0.70 0.71 0.28 0.42 0.42 0.42 0.42 0.43 0.43 0.43	0.40 0.40 0.40 0.57 0.57 0.57 0.57 0.56 0.20 0.35 0.33	0.50 0.27 0.61 0.47 0.30 0.33 0.47 0.45 0.48 0.48 0.48 0.48 0.48 0.48 0.80
Through (m)	0.15 - - 0.60 0.45 0.67 - -	0.20 0.52 0.44 0.28 0.28 0.23 0.23 0.23 0.23 0.23 0.23 0.45 0.45 0.45	0.57 0.47 0.67 0.67 0.67 0.67 0.67 0.67 0.23 0.25 0.25 0.25 0.20 0.17 0.20 0.20 0.20 0.20 0.31 0.31 0.32	0.40 0.45 0.80 0.81 0.64 1.81 0.87 0.34 0.34 0.35 0.31 0.65 1.05
Depth Inside Shear (m)	0.22 0.42 0.15 NVA 	N/A  N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	NNA NNA NNA NNA NNA NNA NNA NNA NNA NNA	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A
Outside Shear (m)	0.93 0.32 0.38 0.38 0.38 1.05 1.00 1.10 0.94 1.10	0.50 - - 1.43 0.90 1.95 0.95 1.15 1.16 1.17 1.05 0.94	$\begin{array}{c} 1.20\\ 1.15\\ 1.15\\ 1.15\\ 1.15\\ 1.20\\ 1.20\\ 1.20\\ 1.20\\ 1.20\\ 0.60\\ 1.20\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 0.85\\ 1.18\\ 0.85\\ 1.22\\$	1.00 0.70 0.70 1.12 1.18 1.12 1.12 0.94 0.94 1.12 1.45 0.90 1.50
Discnarge = : u/s 2/3 ext. (m)	0.50 0.85 0.71 1.00 	0.20 0.88 0.87 0.75 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76	0.90 1.15 0.71 0.71 0.66 0.66 0.97 0.86 0.97 0.86 0.97 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.6	0.63 0.65 0.65 0.75 0.75 0.71 1.11 1.17 1.17 1.17 0.85 0.90 0.90 0.90
0, 1993): s 1/3 ext. (m)	0.15 0.27 0.42 0.53 0.53 0.60 -	cc.0 - 0.76 0.76 0.76 0.36 0.55 0.55 0.55 0.57 0.57 0.52 0.57	0.65 0.90 0.86 0.45 0.45 0.45 0.45 0.47 0.45 0.45 0.45 0.46 0.33 0.46 0.33 0.30 0.30 0.30 0.30 0.30 0.30 0.3	0.32 0.32 0.30 0.35 0.35 0.35 0.35 0.55 0.55 0.55
Site Number Number	LM15.6RAS MC15.7PP MC15.7PP RM16.5RPP RM16.5RPC RM16.5RDC RM16.4PD RM17.1PB RM17.1PB RM17.1PB	KM17595 LM1758C LM183RDC LM213RDC LM213RDC LM213RDC LM213RDC LM2248SBC LM226RDC LM226RDC LM2238SBDC LM2238SBDC LM2238SBDC LM2238SBDC	RM25.0RDC LM24.2RDC LM24.3RDC RM24.3FB RM24.4FC RM24.4FC RM24.4FC RM24.4FC RM24.4FU RM25.4RDC RM25.7RDC RM25.4RDC RM25.4RDC RM25.4RDC RM25.4RDC RM25.4RDC RM25.4RDC RM31.0PBL RM31.4PBL RM31.4PB RM31.4PBL RM31.4PDC RM32.4PDC RM33.4PDC RM32.4PDC RM33.4PDC RM3	LM72.9HAS LM73.0HAS RM74.1HAS LM75.9HAS LM75.9HAS LM80.2HAS LM80.2HAS LM80.2HAS LM80.2HAS LM82.2RAS LM82.3RAS LM83.0RDC MC85.6RDC MC85.6RDC
Spring 1993 / Location (km)	Reach 2 15.6 15.7 15.8 15.8 16.5 16.5 16.8 16.8 17.15 17.3 17.3	21.79 17.99 18.79 20.65 21.4 21.4 21.4 22.5 22.5 22.5 22.5 22.5 22.5 22.5 22	23 242 243 244 244 244 254 254 254 254 254 254 254	72.9 73 75.9 75.9 75.9 80.2 80.2 82.1 82.1 82.3 82.3 82.3 85.3 85.7

Table B1a Spring 1993 Assessment of Habitat Complexing Structures

	1																	-																																		
Substrate B C G F	с -		2 1 3 -	- 12-	321-		3 1 - 3 - 1 - 3 - 2	- 3 1 2	•	3 1 2 -	- 1 2 3	- 2 1 3	- 1	2 1 3 -	- 3 1 2	- 2 3 1	- 3 2 1		· ·	- 1 -	- 1 2 -	- 3 1 2	- 3	- 3 1 2	2 1 3 -	- 3 1 2	3 1 2 - 2 2 2		- 1 2 -	- 3 2 1	 - -	 - 1 - 3	2 1	- 2 3 1	, - -	3 1 - 2	. 1 .	3 1 - 2	- 1 3 2		- 1 - 1 - 2 - 3 - 3	- 2 3 1	- 1 - 2	2 1 3 -		 	- 3 1 2					
Erosion/Sedimentation	M.º	No	No	No	No	NO	ON1	No		No	No	No	No	No	Fines behind RDC	Some fines behind lodge	No No	LITTLE TITLES D/S OF KLDC No	No	No	No	No	No	No	Erosion around outer and inner edges	No	No	No	No	No	No	No	Behind debris pile muddy	No	No	No	No	No	No	NO Erocion in front of DDC and sides		Fines behind (D/S) of SWPR	No	Erosion under and around RDC	Erosion under and around No.	Einas hahind PDC arosion under outer section	Erres benning NDC, erosion under outer section Erosion under and around					
Debris Entrapment	Var	No	Yes	Yes	Yes	No	No	Yes	,	Yes	Yes	Yes	Yes Yes	No 1	Yes	Yes	Yes	Y es No	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	No	Lost	Lost	No	Yes	Yes	No	No.	No	No	°N ;	N0 Vac	Yes	No	No	Yes	Yes Vac	Vac	Yes					
Cover to Bottom?	, var	<u>-</u>	Floating	Yes	Floating			Yes		Yes	Yes	Yes	Yes Yes	Floating	Yes	Yes	Floating	Yes Floating	Yes	Yes	Yes	Yes	Yes	Floating	Yes	Yes	Floating Var	Yes	Floating	Yes	Floating	Floating	Floating	Yes	Floating	Floating	Yes	Floating	Floating	Floating Vac	Floating	Floating	Floating	Yes	Yes Floating	Vac	Yes					
Attached to Shore?	Vac	- 109	Yes	No	No			Yes		No	Yes	Yes	No Yes	No	Yes	Yes	Yes	No Yes	No	Yes	No	Yes	Yes	Yes	No	No	No	Yes	No	Yes	Yes	Yes	Yes	Yes	Vac	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	No :	No No	Vac	No					
Ext. from Margin (m)	00		11.0	6.7	7.5	1.1	0.0 2.6	10.4		8.7	6.7	7.6	C.01 8.7	12.6	7.0	8.0	7.7	C.01	10.0	10.8	15.5	2.2	0.0 8.3	7.4	12.3	6.6	5.5	8.0	7.0	5.0	3.0	C.7	15.0	57.0	5 9	3.0	6.0	9.0	3.0	0.5	6.c1 8.4	6.0	6.0	12.0	570	2.01	21.0	н.				
Cover Area (m <sup>2</sup> )	6	6	14	7	13			32	96	46	49	8 1	1	43	35	136	4 :	18	21	82	24	69 [	81	58	52	10	30	127	21	14	11	75 72	16	192	91	13	2	45	∞;	9 F	32	31	20	7	- 4	0 5	142	G = cohble	G = gravel	F = fines		
d/s 2/3 ext. (m/s)	000		0.46	0.01	0.27			0.18		0.00	0.00	0.10	0.00	0.43	0.05	0.04	0.18	0.00	0.00	0.00	0.00	0.12	00.0	0.04	0.09	0.05	0.05	0.0	0.01	0.40	0.52	0.07	0.00	·	0.50	0.43	0.09	0.30	0.22	0.10	0.61	0.30	0.25	0.55	0.07 Too Deen	100 Deep	0.03					
d/s 1/3 ext. (m/s)	000		0.18	0.20	0.08			0.19		0.25	0.00	0.18	0 00 0	0.18	0.03	0.00	0.39	0.06	0.06	0.09	0.18	0.09	0.00	0.00	0.01	0.11	0.04	00:0	0.03	0.06	0.21	0.14	0.07	·	0.44	0.16	-0.04	0.02	0.14	00:0 82:0	0.45	0.10	0.04	0.28	10.0	0.70	0.58	sam etream	wailable			
Through (m/s)	00.0		0.19	0.02	0.17			0.31		,	0.08	0.00	0.20	0.38	0.05	0.28	0.39	/1/0 N/A	0.31	0.04	0.04	0.04	0.09	0.19	0.02	N/A	0.17	07.0	0.02	0.06	0.21	0.04	0.30		014	0.21	N/A	0.38	0.08	0.05	0.52	0.13	0.09	0.20	02.0	0.00	0.25	u/s = upstre A/s = down	N/A - Not a			
Velocity Inside Shear (m/s)	120		0.45	N/A	N/A			N/A	0.00	0.18	N/A	0.47	0.38 N/A	60.0	N/A	N/A	N/A	0.27 N/A	0.45	N/A	0.48	N/N	A/N	0.19	0.13	0.61	09.0	N/A	0.01	N/A	N/A	A/N	N/A	0.56	N/A	N/A	N/A	N/A	N/A	A/N 97.0	0/.0	N/A	N/A	0.68	0.16	01.0	0.36					
Outside Shear (m/s)	ç	0.29	0.91	0.76	0.78	0.80	0.81	0.36		0.82	0.79	0.77	1 80	0.67	0.55	0.62	0.64	0./8	1.09	0.95	0.56	0.10	75-0	0.32	0.79	0.47	0.73	0.25	0.50	0.50	0.70	0.53	0.91	0.56	0.56	06.0	0.19	0.57	0.41	/ 970 0 00	0.56	0.13	0.45	1.11	175	070	0.98					
u/s 2/3 ext. (m/s)	010		0.54	0.51	0.26			0.24		0.54	0.73	0.33	0.60	0.52	0.56	0.26	0.15	0.46	0.61	0.58	0.19	0.24	0.46	0.20	0.44	0.44	0.62	0.32	0.72	0.35	0.32	0.35			0.41	0.21	0.57	0.39	0.05	0.76	0.29	0.05	0.47	1.17	08.0	76.0	0.60					
u/s 1/3 ext. (m/s)	0.15		0.31	0.19	0.00			0.22	,	0.20	0.55	0.09	0.30	0.38	0.45	0.06	0.07	0.17	0.10	0.01	0.13	0.07	0.28	-0.12	0.26	0.35	0.31	0.07	0.74	0.17	0.26	0.14 0.14	0.12	,	90.0	-0.23	0.16	0.12	-0.05	12.0	0.06	0.02	0.27	1.14	0.80	0.15	0.49	ebris catcher nnel	boom	ar.	pool	
d/s 2/3 ext. (m)	140	14-0	0.63	1.10	0.80			0.30	,	0.73	1.04	1.03	0.75	0.56	0.60	0.70	0.80	0.80	0.83	1.00	0.85	0.70	0.00	1.10	1.12	0.40	0.80	0.92	0.63	0.92	1.20	0.25	1.40		0	0.55	0.98	0.77	0.40	1.30	0.075	0.75	0.95	0.55	1.00 Too Deen	100 Des	06.0	RDC = rail d SC= side cha	DB = debris l	PB = point ba	PP = pocket	
d/s 1/3 ext. (m)	010		0.27	0.30	0.51			0.26		0.41	0.50	0.36	0.48	0.36	0.28	0.37	0.31	0.40	0.53	0.35	0.65	0.50	0.20	0.58	0.80	0.41	0.40	0.30	0.40	0.44	0.75	0.25	0.35	,	0.70	0.35	0.58	0.47	0.21	0.00	0.27	0.35	0.45	0.55	1.00	0.45	0.66					
Through (m)	010		0.60	0.55	0.42			0.30			0.10	0.60	160	0.72	09.0	0.40	0.31	0.40 N/A	0.38	0.45	0.57	0.40	0.75	0.25	1.20	N/A	0.25	0.25	0.35	0.44	0.75	070	0.23		0.75	0.58	N/A	0.75	0.47	0.50	0.15	1.15	0.45	0.70	0.40	0.45	0.92				10.00	per
Depth Depth Inside Shear (m)	200		0.82	N/A	N/A			N/A	0.51	0.17	N/A	0.27	0.45 N/A	0.13	N/A	N/A	N/A	0.27 N/A	0.15	N/A	0.20	N/N	A/N	0.25	0.60	0.62	0.15 N/A	N/A	0.15	N/A	N/A	N/A	N/A	1.10	N/A	N/A	N/A	N/A	N/A	A/N	N/A	N/A	N/A	1.00	c0.1	00'0	0.20			odge	veeper	chored swee catcher
Outside Shear (m)	001	0.17	1.10	1.15	1.10	0.80	0.63	0.35		>1.00	1.40	1.73	0.67	1.15	1.23	1.20	1.10	c0.1	1.14	1.35	1.03	0.75	1.00	1.30	>2.00	0.55	0.80	1.40	0.72	0.93	1.60	0.00	2.00	1.20	1 40	0.75	1.20	1.15	0.80	007<	0.95	1.15	0.95	1.20	ر I.80 م	200	>2.00	/ad sweeper	ng crib	ido beaver le	anchored sv	d-piaced au e-pile debris
u/s 2/3 ext. (m)	0.55	- -	0.77	0.81	0.75			0.35		1.08	0.93	0.75	0.80	0.86	0.45	0.92	0.80	0.83	0.91	1.06	0.94	0.50	0.02	1.00	0.74	0.65	0.27	0.93	0.33	0.75	0.88	0.05	1.06		0.08	0.74	0.50	0.75	0.76	1 00	1.10	1.15	0.78	0.85	96:0 00 5	1 20	1.00	RS = rootw RP = hrush	FC = floati	PBL = pset	RAS = rail	PDC = pipe
22 - 23, 13 u/s 1/3 ext. (m)	100	100	0.48	0.50	0.45			0.26		0.40	0.50	0.50	050 050	0.51	0.25	0.36	0.46	02.0	0.50	0.59	0.52	0.35	0.31	0.25	0.43	0.62	0.16	0.57	0.23	0.35	0.50	0.25	0.57		0.48	0.30	0.25	0.30	0.30	cc.0	0.75	0.80	0.43	0.70	06.0	0.48	0.06					
4 Assessment ( May Site Number	3V d9 51M 1	MC15.7PP	RM16.2RAS	RM16.5RDC	RMI6.8RDC	KM17.15PB	RM17.3PB	RM17.9DB	RMI7.9SC	LM18.3RDC	RM20.65RDC	LM21.3RDC	RM22.0RDC	RM22. IRAS	RM22.55RDC	LM22.6RDC	LM22.7RDC	RM22.95RAS	RM23.0RDC	LM24.2RDC	LM24.3RDC	RM24.35RS	RM24.6PBL	RM24.8PBL	RM25.4RDC	MC25.7RDC	RM26.9RAS	RM28.4RDC	LM29.4RAS	RM31.0PBL	RM31.1PBL	LM32.65HAS	RM34.7PDC	MC35.4PDC	SAHP CTM I	LM73.0HAS	RM74.1HAS	LM75.9HAS	LM78.0HAS	LM80.2HAS	LM82.IRAS	LM82.2RAS	LM82.3HAS	LM83.0RDC	MIC85.0KDC RM85 7P AS	P M86 35P DC	RM86.375RDC	RM = right margin MC = mid-channel	LM = left margin	2		
Spring 195 Location (km)	Reach 2	15.7	16.2	16.5	16.8	17 15	17.3	17.9	17.9	18.3	20.65	21.3	4.12 22	22.1	22.55	22.6	22.7	22.95	23	24.2	24.3	24.35	24.6	24.8	25.4	25.7	26.9 27.4	28.4	29.4	31	31.1	32.65	34.7	35.4	Reach 4 77 9	73	74.1	75.9	78	80.9	82.1	82.2	82.3	83	0.C8 7.58	86.35	86.375	Where,				

Table B3 Spring 1994 Assessment of Habitat Complexing Structures

Table B3.
Spring 1994 Assessment of Habitat Complexing Structures

Site				
Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
LM15.6RAS	No	No		
MC15 7PP	No	No	-	
RM162RAS	No	No	Vary little debris entrement smell branches	Sweener still intact
RM16 5RDC	No	No	very nue deons entraphient, sman oranches	-
RM16 8RDC	No	No	-	
RM17 0PB	No	No	-	
RM17 15PB	No	No	-	-
RM17 3PB	INO N-	No	-	-
RM17.0DB	INO N-	No	-	- Dobris boom in good shape
PM17.9DD	No	No	-	Debris boom in good snape
L M18 2PDC	No	No	-	- Desver Ledes
EM10.5RDC	No	No	-	
LM21 2DDC	No	No	-	Good stable debris pile
LM21.3RDC	No	No	-	-
LM21.4RDC	No	No	-	Good stable debris pile
RM22.0RDC	No	No	-	Good stable debris pile
RM22.1RAS	Branches on D/S side of SWPR only	No	Very little debris trapped	Sweeper in good shape
RM22.55RDC	No	No	-	RDC, stable debris pile
LM22.6RDC	No	No	-	Beaver lodge, very stable RDC
LM22.7RDC	No	No	-	RDC U/S is affecting flows here
LM22.85RDC	No	No	-	Stable RDC
RM22.95RAS	SWPR is broken, few branches left on them	No	-	New SWPR needed
RM23.0RDC	No	No	-	Good stable RDC and debris
LM24.2RDC	No	No	-	Old beaver lodge
LM24.3RDC	No	No	Smaller type of entrapment debris gone at high water	Structurally sound
RM24.35RS	Two separate complexes now	No	-	-
RM24.4FC	No	No	-	Structurally sound
RM24.6PBL	No	No	-	Good sound structure
RM24.8PBL	Debris weak, gone at high water	No	-	Structure sound
RM25.4RDC	No	No	90% of debris on U/S side of rails	Debris wash off at high flows
MC25.7RDC	Ne	No		All the debris looks like it was placed and is holding
RM26 9RAS	INU No branches on SW/DP	INO No	-	Debris will be lost at high water
	Site Number	SiteDamageLM15.6RASNoMC15.7PPNoRM16.2RASNoRM16.2RASNoRM16.5RDCNoRM16.6RDCNoRM17.0PBNoRM17.15PBNoRM17.3PBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM17.9DBNoRM2.065RDCNoLM21.3RDCNoRM22.0RDCNoRM22.0RDCNoRM22.0RDCNoRM22.5SRDCNoRM22.5SRDCNoRM22.9SRASSWPR is broken, few branches left on themRM23.0RDCNoLM24.2RDCNoRM23.0RDCNoRM24.3FRSTwo separate complexes nowRM24.4FCNoRM24.4FCNoRM24.4FCNoRM24.4FDNoRM24.4FDNoRM24.4FBLDebris weak, gone at high waterRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDLNoRM24.4FDL <td>Site     Danage     Displacement       LM15.6RAS     No     No       RM16.2RAS     No     No       RM16.2RAS     No     No       RM16.5RDC     No     No       RM16.5RDC     No     No       RM17.0PB     No     No       RM17.15PB     No     No       RM17.3PB     No     No       RM17.3PD     No     No       RM20.6SRDC     No     No       RM20.6SRDC     No     No       RM21.4RDC     No     No       RM22.5SRDC     No     No       RM22.</td> <td>Site NumberDamageDisplacementDebris Accumulation/LossLM15.0RASNoNo.MC15.7PPNoNoVery little debris entrapment, small branchesRM16.5RASNoNoVery little debris entrapment, small branchesRM16.5RACNoNo.RM17.0PBNoNo.RM17.0PBNoNo.RM17.1SPBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM20.6SRDCNoNo.RM20.6SRDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNo</td>	Site     Danage     Displacement       LM15.6RAS     No     No       RM16.2RAS     No     No       RM16.2RAS     No     No       RM16.5RDC     No     No       RM16.5RDC     No     No       RM17.0PB     No     No       RM17.15PB     No     No       RM17.3PB     No     No       RM17.3PD     No     No       RM20.6SRDC     No     No       RM20.6SRDC     No     No       RM21.4RDC     No     No       RM22.5SRDC     No     No       RM22.	Site NumberDamageDisplacementDebris Accumulation/LossLM15.0RASNoNo.MC15.7PPNoNoVery little debris entrapment, small branchesRM16.5RASNoNoVery little debris entrapment, small branchesRM16.5RACNoNo.RM17.0PBNoNo.RM17.0PBNoNo.RM17.1SPBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM17.3PBNoNo.RM20.6SRDCNoNo.RM20.6SRDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.RM22.0RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNoNo.LM22.4RDCNo

Table B3.
Spring 1994 Assessment of Habitat Complexing Structures

Location	Site				
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
27.4	DM07 4EC				Floating crib structure is solid, FC middle is open, half of FC
27.4	KM27.4FC	No	No	Not much debris on structure	out of water
28.4	RM28.4RDC	No	No	-	Solid complex
29.4	LM29.4RAS	SWPR broken between rails, velocity too fast	No	-	New SWPR needed ?
31.0	RM31.0PBL	No	No	No debris entrapment	Structure together
31.1	RM31.1PBL	No	No	Very little debris caught	Structure sound
31.4	RM31.4BP	No	No	-	-
32.65	LM32.65HAS	No	No	-	SWPR in good shape
34.7	RM34.7PDC	No	No	-	Solid debris pile
35.4	MC35.4PDC	No	No	-	-
Reach 4					
72.9	LM72.9HAS	No	No	Some small debris trapped in branches of SWPR	SWPR still in good shape
73.0	LM73.0HAS	SWPR broken	No	-	New SWPR needed
74.1	RM74.1HAS	SWPR is just a pole no branches	No	Some debris is piled up on the shore, cover at higher water	No cover provided
75.9	LM75.9HAS	No	No	-	SWPR's are in good shape
78.0	LM78.0HAS	No	No	-	SWPR in good shape
80.2	LM80.2HAS	No branches on SWPR	No	-	SWPR does provide some cover
80.9	LM80.9RDC	No	No	-	-
82.1	LM82.1RAS	No	No	-	SWPR in good shape
82.2	LM82.2RAS	No	No	-	-
82.3	LM82.3HAS	No	No	-	SWPR in good shape, natural SWPR 1m D/S of site SWPR
83.0	LM83.0RDC	No	No		-
85.6	MC85.6RDC	No	No		-
85.7	RM85.7RAS	No	No	-	SWPR holding OK
86.35	RM86.35RDC	No	No		RDC in good shape
86.375	RM86.375RDC	No	No	-	Good stable RDC
Where,	RM = right margin	RS = rootwad sweeper	u/s = upstream		
	MC = mid-channel	BP = brush pile	d/s = downstream		
	LM = left margin	FC = floating crib	N/A - Not available		

Table B4 Spring 1995 Assessment of Habitat Complexing Structures

Spring 1995 Assessment ( May 16 - 18, 1995): Discharge = 62.3 m<sup>3</sup>/s (2,200 cfs)

nate G F	3	3	' (1 (	- 1	2 3	0 0 0 0	n 7 7	1 2		5 3 5 3		- 1 - 0 - 0	2 3	2	· c · -	1 m	1 3	1 3	. 3			3 1	2 1	2	- 7 - 7	 	- C	2 1	1 2	- 1	 4 -		1 3		- 12		1 2	2 1	, , , ,	0 C	- 1	1 2				
Subst B C	-	2 1	 ~ ~	- 6	-		- n	, 1	- 2	- , ,	, ,	7 7 	-	ŝ		. 6	- 2	- 2	- 2			-	1		, c ,	، ر ا	4 i i i	;	ļ	. "	• • • •	- C - C	- 2	ļ	;		1	; ;	, ,	-		. 3				
Eresion/Sedimentation	ΝοΝο	NA	No/No	Erosion, and Silts u/s of SWPR	No/No	No/No	NA No erosion/ a little silt d/s of DB	NA	No/No	No/No	Erosion outside of RDC/ No sedimentation	Erosion on bour sides of KDC/ No sedim. Erosion outside edge of RDC/ No sedim.	No/No	No/No	Erosion outside of KUC/ No sedim'n No/No	N/N	No/No	No/No	No/No	No erosion/ silt deposition	No/No No/No	Erosion around and under RDC/ No sedim'n	No/No	No/No	No/No No/No	N/NO NO/NO	No/No	No/No	No/No	No/No No acceion/ Silt hadind DDC		ON/ON	No/No	No erosion/ silt d/s of SWPR	No erosion / sediment'n behind SWPR	Erosion around ed ge/ No sediment	No/No	No erosion / Some silt	N/NO	Erosion around KUC / No sediment n Nic/Nic	Erosion outside of RDC/ Silt behind complex	Erosion each side of RDC / Sediment behind RDC				
Debris Entrapment	~	z	z>	۲.	NA	NA	Y Y	NA	Y	У;	Y	××	z	۲ ;	×	Z	Υ	Y	Y	×	- >	×	Υ	Y	×	× 2	2 7	NA	z	7 >	-	7	Z	Y	ZŽ	2 <b>&gt;</b>	Z	z	AN Y	- >	- ×	Y				
Cover to Bottom?	×	Y	ZZ	Υ Υ	NA	AN	ΥN	NA	Y	Υ;	Υ.	× ×	Υ	Υ:	× >		Υ	Y	Υ;	×	- >	z	Υ	z	×	* >	- z	Y	Y	¥ >	-	z	Υ	z	¥	- z	z	Y	×	- 2	z >	Υ				
Attached to Shore?		,	ı.						,								ı																		,	. ,						,				
Ext. from Margin (m)	10.00	N/A	06.6	0.20			12.00	N/A	6.60	6.00	00.11	9.20	1.00	9.00	8.00	N/A	10.60	13.50	8.70	10./0	0.00	16.10	N/A	8.00	6.20	1 40	N/A	2.60	3.60	11.90	07:70	6.00	3.20	7.50	N/A	A/A	N/A	5.00	6.00	13.00	0.00 9.60	N/A				
Cover Area (m <sup>2</sup> )	50	NA	50	21	NA	AN NA	60 N	NA	57	36	81 2	61	9	49	136 20	ì	42	137	26	8 5	16 05	4	10	54	53	711	21	4	ŝ	42	Ê	4	9	15	61 (	n oc	5	9	× :	= •	12 %	10				
d/s 2/3 ext. (m/s)	0.00	,	0.66	00:0		,	- 00.00		0.07	0.00	0.00	60.0 00.0	0.10	0.00	0.00	0.51	0.00	0.00	0.01	60.0	0.46	0.10	0.33	0.19	0.15	0.00	1.27	0.00	0.32	0.00	00.0	0.32	0.00	0.13	0.37	0.02	0.16	0.01	0.31		- 0.03	0.49				
d/s 1/3 ext. (m/s)	0.06	,	0.41	0.38			- 0.09	'	0.02	0.00	0.19	0.00	,	0.00	0.00	0.20	0.03	0.05	0.50	10.0	0.01	0.09	0.34	0.01	0.00	0.00	0.22	0.00	0.28	0:00	000	0.02	0.02	0.00	0.20	0.56	0.46	-0.09	0.12	0.50	0.02	0.25				
Through (m/s)	0.30		0.70	0.47			- 0.01	0.00	0.02	0.08	, 00	0.01	,		- 031		,	0.02	0.01	0.14		0.13	0.01	0.36	0.07		,	0.00	0.23	0.06		0.22	0.09	0.25	,	0.22	0.18	0.14	0.06	0.04	0.46	0.01				
elocity Inside Shear (m/s)			- 16	0.28					,		0.31		,		- 14	ļ.,	0.24		0.17	77.0		0.04	0.37							- 0.61	10:0		,	,	,	- 0.62		,	- 170	14:0 14:0	0.40	0.63				
V Outside Shear (m/s)	0.40	,	0.71	0.84			- 0.41		0.52	0.89	0.69	0.37 1.37	0.12	0.74	05.0	0.71	0.66	0.63	0.34	0.50	0.59	0.54	0.81	1.01	0.66	0.79	0.72	0.43	0.55	0.75		0.31	0.33	0.58	0.33	0.51	0.99	0.27	0.56	201	0.86	0.48	B = boulder C = cobble G = gravel F = fines			
u/s 2/3 ext. (m/s)	0.54	,	0.66	0.32			- 0.15		0.33	0.53	0.42	0.78	00.0	0.40	0.00	0.67	0.81		0.03	01.0	0.01	0.56	0.46	0.68	0.30	70.0	0.55	0.26	0.19	0.53	600	0.12	-0.11	0.16	0.05	01-10	0.30	0.12	0.12	c0.1	- 0.27	0.66				
u/s 1/3 ext. (m/s)	0.13	,	0.49	00.0			- 0.25		0.00	0.56	0.00	0.37	,	0.22	0.24	0.24	0.28	0.04	0.00	0.00	- 000	0.24	0.45	0.35	0.13	0.41	0.01	0.15	0.22	0.48	67.0	0.00	-0.12	0.10	0.00	- 0.59	0.15	0.04	0.16	0.65	0.00	0.32	m ream ailable			
d/s 2/3 ext. (m)	0.29	,	0.73	0.78			- 0.38		0.59	1.00	0.96	c/ .0 19:0	0.15	1.05	0.80	0.50	0.80	0.82	0.77	0.70	0.75	0.60	0.40	0.65	0.31	02.0	0.87	0.48	0.44	0.66	0	0.64	0.50	0.70	0.60	75.0	0.65	0.60	0.47		- 0.70	1.05	u/s = upstreau d/s = downsti N/A - Not av			
d/s 1/3 ext. (m)	0.15	,	0.40	0.49			- 0.30		0.18	0.51	0.38	0.38		0.50	0.34	0.50	0.44	0.38	0.65	0.00	0.45	1.00	0.30	0.46	0.26	10.0	0.41	0.50	0.17	0.35	6000	0.40	0.32	0.40	0.30	0.39	0.28	0.20	0.25	0.47	0.81	0.40				
Through (m)	0.20		0.72	0.46	,		0.30	0.58	0.18	0.15	, ,	0.75	,	ŀ	- 17 0		ī	0.24	0.65	0./1		1.80	0.55	0.54	0.35		,	0.36	0.26	0.44		0.59	0.50	0.74		0.85	0.80	0.80	0.23	0.80	09.0	1.05				
Depth Inside Shear (m)		,	- 10	0.12							0.38		,		- 030	-	0.20		0.20	0.20		0.15	0.40								CO-1	,	,			0.75	Ţ		- 100	0.54	+C-0	1.20	dge eeper	hored sweepe catcher er		
Outside Shear (m)	16.0		1.02	1.10			- 0.44		1.26	1.80	1.20	0.90	0.29	1.00	1 23	1.10	1.20	1.30	1.00	c/ .0	1.001	2.00	0.50	0.88	0.98	02.1	1.35	1.10	0.59	1.50	00-1	060	0.86	1.18	1.12	1.14	1.40	1.26	0.93	1.65	1.90	1.50	sweeper le crib beaver lo chored sw	laced and ile debris bris catch	oom	loo
u/s 2/3 ext. (m)	0.65		0.90	0.84		,	- 0.36		0.97	1.30	0.82	c/ .0 06.0	0.16	1.10	1.20	0.95	1.05	0.85	0.44	c/.0	0.73	0.91	0.65	0.55	1.23		1.04	0.61	0.38	1.23	1711	0.75	0.51	0.70	0.70	1.00	0.84	0.54	0.65	0.08	1.10	0.88	RS = rootwad BP = brush pi FC = floating PBL = pseudd RAS = rail-ar	HAS = nanu- PDC = pipe-F RDC = rail de	SC= side chai DB = debris t PB = point ba	PP = pocket I
u/s 1/3 ext. (m)	0.30	,	0.65	0.63			- 0.40		0.38	0.75	0.48	0.64 0.64		0.80	0.88	0.50	0.54	0.50	0.47	C0.U	0.35	0.30	0.45	0.30	0.84	- 1	0.72	0.34	0.22	0.79	000	0.38	0.30	0.40	0.32	- 0.75	0.52	0.26	0.26	07.0	0.46	0.35				
Site Number	LM15.6RAS	MC15.7PP	RM16.2RAS	RM16.8RDC	RM17.0PB	RMI7.15PB	RM17.9DB	RM17.9SC	LM18.3RDC	RM20.65RDC	LM21.3RDC	RM22.0RDC	RM22. IRAS	RM22.55RDC	LM22.6KDC	RM22.95RAS	RM23.0RDC	LM24.2RDC	LM24.3RDC	KM24.55KS	RM24.6PBL	RM25.4RDC	MC25.7RDC	RM26.9RAS	RM27.4FC	KM28.4KDC I M79.4RAS	RM31.1PBL	RM31.4BP	LM32.65HAS	RM34.7PDC MC35 ADDC	OG H-COW	1.M72.9HAS	LM73.0HAS	LM75.9HAS	LM78.0HAS	LM80.9RDC	LM82.1RAS	LM82.2RAS	LM82.3HAS	DM85.UKDC	RM86.35RDC	RM86.375RDC	RM = right margin MC = mid-channel LM = left margin			
Location (km)	Reach 2 15.6	15.7	16.2 16.5	16.8	17	17.15	17.9	17.9	18.3	20.65	21.3	22	22.1	22.55	22.6	22.95	23	24.2	24.3	24.55	24.6 24.6	25.4	25.7	26.9	27.4	20.4 20.4	31.1	31.4	32.65	34.7 35.4	t -	Reach 4 72.9	73	75.9	78	2.00 80.9	82.1	82.2	82.3	65 7 29	86.35	86.375	Where,			

## Table B4 Spring 1995 Assessment of Habitat Complexing Structures

Spring 1995 Assessment (May 16 - 18, 1995): Discharge = 62.3 m<sup>3</sup>/s (2,200 cfs)

(hm)NumberDamageDisplacementDehris Accumulation/LossRecommendation/Comments156IM15 SPAS157MC15 S7PP153MC15 S7PP154MC15 S7PS155MK16 SRDC158RM16 SRDC157RM17 S7B <td< th=""><th>Location</th><th>Site</th><th></th><th></th><th></th><th></th></td<>	Location	Site				
Rach 2         . <td>(km)</td> <td>Number</td> <td>Damage</td> <td>Displacement</td> <td>Debris Accumulation/Loss</td> <td>Recommendation/Comments</td>	(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
Retar         . <td>Derek 2</td> <td></td> <td></td> <td></td> <td></td> <td>_</td>	Derek 2					_
11.10       LM1.3 MCJS       -       -       -       -         16.2       RM16.3 RAS       No bark, branches on d's side of SWPR       -       -         16.5       RM16.8 RAC       -       -       Lacose debris, gone at higher flows       -         16.8       RM16.8 RAC       -       -       -       -         17.1       RM17.15PB       -       -       -       -         17.3       RM17.15PB       -       -       -       -         17.4       RM17.15PB       -       -       -       -       -         17.3       RM17.3PB       - </td <td></td> <td>IM15 CDAS</td> <td></td> <td></td> <td></td> <td></td>		IM15 CDAS				
15.2       NRC15.PP       ·       ·       ·       ·       ·       ·         16.2       RMI 62RAS       only       ·       ·       ·       ·         16.5       RMI65RDC       ·       ·       Loose debris, gone at higher flows       ·         16.5       RMI67RDC       ·       ·       ·       ·       ·         17.15       RMI7.0FB       ·       ·       ·       ·       ·       ·         17.9       RMI7.0FB       · </td <td>15.0</td> <td>LWI15.0KAS</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td>	15.0	LWI15.0KAS	-	-	-	-
Inclusion       Not barry output on the state of NWPR output on the state	15.7	MC15./PP		-	-	-
June 2         June 2 <thjune 2<="" th=""> <thjune 2<="" t<="" td=""><td>16.2</td><td>RM16.2RAS</td><td>No bark, branches on d/s side of SWPR</td><td></td><td></td><td></td></thjune></thjune>	16.2	RM16.2RAS	No bark, branches on d/s side of SWPR			
10.10       NM10, ND,       -       -       Loose devise, goint a largien nows       -         17       RM10, SPDC       -       -       -       -         17       RM17, SPB       -       -       -       -         17.15       RM17, SPB       -       -       -       -         17.3       RM17, SPB       -       -       -       -         17.9       RM17, SPB       -       -       -       -         17.9       RM17, SPB       -       -       -       -       -         17.9       RM17, SPB       -	165	DM16 5DDC	only	-	- Loose debrie, gone at higher flows	-
Init       Knill skuble       -       -       -         17       Knill 7,9PB       -       -       -         17.13       Knill 7,9PB       -       -       -         17.3       Knill 7,9PB       -       -       -         17.3       Knill 7,9PB       -       -       -         17.9       Knill 7,9PB       -       -       -         17.9       Knill 7,9PB       -       -       -       -         18.3       LMI8,3RDC       -       -       -       -       -         20.6       RM20,6KBDC       - <t< td=""><td>10.5</td><td>RM16.5RDC</td><td>-</td><td>-</td><td>Loose debris, gone at higher nows</td><td>-</td></t<>	10.5	RM16.5RDC	-	-	Loose debris, gone at higher nows	-
17.15       KN17.15PB       -       -       -       -         17.15       KN17.15PB       -       -       -       -         17.3       KN17.3PB       -       -       -       -         17.9       KN17.9DB       -       -       -       -       -         17.9       KN17.9DB       -       -       -       -       -       -         17.9       KN17.9DB       - </td <td>10.8</td> <td>DM17 ODD</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td>	10.8	DM17 ODD	-	-	-	-
17.3       RM17.3PB       -       -       -         17.3       RM17.3PB       -       -       -         17.9       RM17.3PB       -       -       -         17.9       RM17.3PB       -       -       -         17.9       RM17.9PB       -       -       -         17.9       RM17.3PB       -       -       -         17.9       RM17.3PB       -       -       -         17.9       RM17.3PB       -       -       -       -         18.3       LM18.3RDC       -       -       -       -       -         21.4       I.M21.4RDC       -	17.15	KM17.0PB	-	-	-	-
11.3       RM17.9DB       -       -       -       -         17.9       RM17.9BC       -       -       -       -         17.9       RM17.9BC       -       -       -       -         18.3       LM18.3RDC       -       -       -       -       -         20.65       RM20.6SRDC       -       -       -       -       -         21.3       LM21.3RDC       -       -       -       -       -       -         21.4       LM21.4RDC       -	17.15	KM17.15PB	-	-	-	-
17.9       RM17.90S       -       -       -       -         17.9       RM17.90S       -       -       -       -         18.3       LM13.3RDC       -       -       -       -       -         20.65       RM20.65RDC       -       -       -       -       -       -         21.3       LM21.3RDC       -       <	17.3	RM17.3PB	-	-	-	-
11.93       KM12-SDC       -       -       -         18.8       LM18-SRDC       -       -       -         20.65       RM20.65KDC       -       -       -       -         21.4       LM21.3RDC       -       -       -       -         21.4       LM21.4RDC       -       -       -       -         22       RM22.0RDC       -       -       -       -       -         22.1       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -       -       -         22.55       RM22.55KDC       -	17.9	RM17.9DB	-	-	-	-
18.3       LM15.MDC       -       -       -         20.65       RM20.65RDC       -       -       -         21.3       LM21.3RDC       -       -       -         21.4       LM21.4RDC       -       -       -         22       RM22.06RDC       -       -       -         22       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -         22.11       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -       -         22.55       RM22.5RDC       -       -       -       -       -       -         22.65       LM22.5RDC       - <td< td=""><td>17.9</td><td>KM17.95C</td><td>-</td><td>-</td><td>-</td><td>-</td></td<>	17.9	KM17.95C	-	-	-	-
21.3       LM21.3RDC       -       -       -       -         21.4       LM21.4RDC       -       -       -       -         21.4       LM21.4RDC       -       -       -       -         22       RM22.0RDC       -       -       -       -       -         22.1       RM22.0RDC       -       -       -       -       -         22.1       RM22.0RDC       -       -       -       -       -         22.5       RM22.6RDC       -       -       -       -       -         22.6       LM22.6RDC       -	18.3	LM18.3RDC	-	-	-	-
1.1.3       LM21.3DC       -       -       -       -         21.4       LM21.4RDC       -       -       -         22       RM22.0RDC       -       -       -       -         22.1       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -         22.55       RM22.5SRDC       -       -       -       -         22.6       LM22.6RDC       -       -       -       -         22.65       LM22.8SRDC       -       -       -       -         22.65       LM22.9SRAS       -       -       -       -         22.85       LM22.9SRAS       -       -       -       -       -         22.95       RM22.9SRAS       -	20.65	RM20.65RDC	-	-	-	-
1.14       LM21 ARDC       -       -       -       -         22       RM20 RDC       -       -       -       -         22.1       RM22.RAS       -       SWPR broken near anchor (outside)       -       -         22.55       RM22.SSRDC       -       -       -       -         22.65       LM22.SRDC       -       -       -       Beaver Lodge         22.85       LM22.SRDC       -       -       -       -         22.95       RM20.9SRAS       -       -       SWPR bare log       -         22.95       RM23.0RDC       -       -       -       -         23       RM23.0RDC       -       -       -       -       -         24.2       LM24.SRDC       -	21.3	LM21.3RDC	-	-	-	-
22       RM22.0RDC       -       -       -       -         22.11       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -         22.55       RM22.5SRDC       -       -       -       -         22.6       LM22.6RDC       -       -       -       -         22.65       RM22.9SRDC       -       -       -       -         22.85       RM22.9SRAS       -       -       -       -         22.95       RM2.0RDC       -       -       -       -       -         22.95       RM2.0RDC       -       -       -       -       -       -         24.2       LM24.2RDC       -	21.4	LM21.4RDC	-	-	-	-
22.1       RM22.1RAS       -       SWPR broken near anchor (outside)       -       -         22.55       RM22.5RDC       -       -       -       -         22.65       LM22.6RDC       -       -       -       Beaver Lodge         22.85       LM22.9SRAS       -       -       -       -         22.95       RM22.9SRAS       -       -       -       -         22.95       RM22.9SRAS       -       -       -       -         24.9       LM24.2RDC       -       -       -       -         24.3       LM24.3RDC       -       -       -       -       -         24.4       RM24.4RDC       -       -       -       -       -       -         24.3       LM24.3RDC       -	22	RM22.0RDC	-	-	-	-
22.55       RM22.55 RDC       -       -       -       Beaver Lodge         22.65       LM22.68DC       -       -       Beaver Lodge         22.85       LM22.88DC       -       -       -         22.95       RM22.95RAS       -       -       -       -         22.95       RM22.95RAS       -       -       SWPR bare log       -         23       RM23.0RDC       -       -       -       -       -         24.3       LM24.3RDC       - <t< td=""><td>22.1</td><td>RM22.1RAS</td><td>-</td><td>SWPR broken near anchor (outside)</td><td>-</td><td>-</td></t<>	22.1	RM22.1RAS	-	SWPR broken near anchor (outside)	-	-
22.6       LM22.6RDC       -       -       Beaver Lodge         22.85       LM22.85RDC       -       -       -         22.95       RM22.95RAS       -       -       -         23.9       RM23.0RDC       -       -       SWPP hare log       -         24.2       LM24.2RDC       -       -       -       -         24.3       LM24.3RDC       -       -       Additional debris       Beaver Lodge         24.3       LM24.3RDC       -       -       -       Lots of silt         24.3       LM24.4RC       -       -       -       -         24.4       RM24.4FC       -       -       -       -         24.6       RM24.6PBL       -       -       -       -         25.4       RM25.4RDC       -       -       -       -         25.7       MC25.7RDC       -       -       -       -       -         26.9       RM26.9RAS       -       -       -       -       -       -         26.9       RM26.9RAS       -       -       -       -       -       -       -       -       -       -       -       - <td>22.55</td> <td>RM22.55RDC</td> <td>-</td> <td>-</td> <td>-</td> <td>-</td>	22.55	RM22.55RDC	-	-	-	-
22.85       LM22.85RDC       -       -       -       -         22.95       RM22.95RAS       -       -       SWPR bare log       -         23       RM23.0RDC       -       -       -       -         24.2       LM24.2RDC       -       -       Additional debris       Beaver Lodge         24.3       LM24.3RDC       -       -       -       Lots of silt         24.3       LM24.4RDC       -       -       -       -         24.4       RM24.4FC       -       -       -       -         24.4       RM24.4FC       -       -       -       -       -         24.4       RM24.4FC       - <t< td=""><td>22.6</td><td>LM22.6RDC</td><td>-</td><td>-</td><td>-</td><td>Beaver Lodge</td></t<>	22.6	LM22.6RDC	-	-	-	Beaver Lodge
22.95       RM22.95RAS       -       -       SWPR bare log       -         23       RM23.0RDC       -       -       -       -         24.2       LM24.2RDC       -       -       Additional debris       Beaver Lodge         24.3       LM24.3RDC       -       -       Lots of silt         24.4       RM24.4SFC       -       -       -       Lots of silt         24.4       RM24.4FC       -       -       -       -       -         24.4       RM24.4FC       -       -       -       -       -       -         24.4       RM24.4FC       -<	22.85	LM22.85RDC	-	-	-	-
23       RM23.0RDC       -       -       -       -         24.2       LM24.2RDC       -       -       Additional debris       Beaver Lodge         24.3       LM24.3RDC       -       -       Lots of silt         24.3       RM24.3RDC       -       -       Lots of silt         24.3       RM24.4FC       -       -       -         24.4       RM24.4FC       -       -       -       -         24.6       RM24.6PBL       -       -       -       -       -         24.6       RM24.6PBL       - <t< td=""><td>22.95</td><td>RM22.95RAS</td><td>-</td><td>-</td><td>SWPR bare log</td><td>-</td></t<>	22.95	RM22.95RAS	-	-	SWPR bare log	-
24.2       LM24.2RDC       -       -       Additional debris       Beaver Lodge         24.3       LM24.3RDC       -       -       Lots of silt         24.3       RM24.35RS       -       -       Lots of silt         24.4       RM24.4FC       -       -       -       -         24.4       RM24.4FC       -       -       -       -         24.6       RM24.6PBL       -       -       -       -       -         24.6       RM24.6PBL       -	23	RM23.0RDC	-	-	-	-
24.3       LM24.3RDC       -       -       Lots of silt         24.35       RM24.3SRS       -       -       -         24.4       RM24.4FC       -       -       -         24.4       RM24.4FC       -       -       -         24.4       RM24.4FC       -       -       -         24.6       RM24.6FBL       -       -       -         25.4       RM25.4RDC       -       -       -         25.7       MC25.7RDC       -       -       -         26.9       RM26.9RAS       -       -       -         27.4       RM27.4FC       Complex ok       -       -       -         28.4       RM28.4RDC       -       -       -       -         29.4       LM29.4RAS       Outside anchor gone       SWPR pushed against shore       -       -         31.1       RM31.1PBL       -       -       -       -       -	24.2	LM24.2RDC	-	-	Additional debris	Beaver Lodge
24.35       RM24.35RS       -       -       -       -       -         24.4       RM24.4FC       -       -       -       -       -         24.6       RM24.6PBL       -       -       -       -       -       -         24.6       RM24.6PBL       -       -       -       -       -       -       -         25.4       RM25.4RDC       -       <	24.3	LM24.3RDC	-	-	-	Lots of silt
24.4RM24.4FC24.6RM24.6PBL25.4RM25.4RDC-Loose debris u/s will be lost at higher flows25.7MC25.7RDC26.9RM26.9RAS27.4RM27.4FCComplex ok28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	24.35	RM24.35RS	-	-	-	-
24.6RM24.6PBL25.4RM25.4RDCLoose debris u/s will be lost at higher flows-25.7MC25.7RDC26.9RM26.9RAS27.4RM27.4FCComplex ok28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	24.4	RM24.4FC	-	-	-	-
25.4       RM25.4RDC       Loose debris u/s will be lost at higher flows       -         25.7       MC25.7RDC       -       -         26.9       RM26.9RAS       -       -       -         27.4       RM27.4FC       Complex ok       -       -       -         28.4       RM28.4RDC       -       -       -       -         29.4       LM29.4RAS       Outside anchor gone       SWPR pushed against shore       -       -         31.1       RM31.1PBL       -       -       -       -       -	24.6	RM24.6PBL	-	-	-	-
25.7MC25.7RDCflows-25.7MC25.7RDC26.9RM26.9RAS27.4RM27.4FCComplex ok28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	25.4	RM25 4RDC			Loose debris u/s will be lost at higher	
25.7MC25.7RDC26.9RM26.9RAS27.4RM27.4FCComplex ok-Very little debris trapped; some sticks-28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	2011	10.1201111200	-	-	flows	-
26.9RM26.9RAS27.4RM27.4FCComplex ok-Very little debris trapped; some sticks-28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	25.7	MC25.7RDC	-	-	-	-
27.4RM27.4FCComplex okVery little debris trapped; some sticks-28.4RM28.4RDC29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	26.9	RM26.9RAS	-	-	-	-
28.4     RM28.4RDC     -     -     -     -       29.4     LM29.4RAS     Outside anchor gone     SWPR pushed against shore     -     -       31.1     RM31.1PBL     -     -     -     -	27.4	RM27.4FC	Complex ok	_	Very little debris trapped; some sticks	-
29.4LM29.4RASOutside anchor goneSWPR pushed against shore31.1RM31.1PBL	28.4	RM28.4RDC	-	-	-	-
31.1 RM31.1PBL	29.4	LM29.4RAS	Outside anchor gone	SWPR pushed against shore	-	-
	31.1	RM31.1PBL	-		-	-

## Table B4 Spring 1995 Assessment of Habitat Complexing Structures

Spring 1995 Assessment (May 16 - 18, 1995): Discharge = 62.3 m<sup>3</sup>/s (2,200 cfs)

Location	Site				
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
21.4	D) (21 (DD				
31.4	RM31.4BP	-	-	-	-
32.65	LM32.05HAS	- T C 1/ 11	SWPR pushed against shore	-	-
34.7	RM34./PDC	Loss of d/s pile	-	Loss of debris due to damage	-
35.4	MC35.4PDC	-	-	-	-
Deach 4					-
Keach 4		Vary little cover and bronches stringed			-
72.9	LM72.9HAS	bara log left			
		bare log left	-	-	-
73	LM73.0HAS	Bara log with bara branches and no bark			
		Date log with bare branches and no bark	-	-	=
75.9	LM75.9HAS				30 cm of silt between S w PK; 40 cm of silt d/s of
79	I M79 OUAS	- Bare logs (3)	-	-	u/s 5 W1 K
78	LM/0.0HA5	Date logs (3)	-	-	-
80.2	LM80.2HAS	Bare log held with lope, bank sturring	Log against hank		Site a lot shallower than last year
80.9		away	Log against bank	- Lost debris from last year	She a fot shahower than fast year
82.1	LM80.9RDC	-	-	Lost debris from last year	- SWPR in reasonable shape
82.1	LM02.TRAS	- Anchor stump broken	-	-	SWPR in reasonable shape
82.2	LM02.2KAS	Anchor stump broken	-	-	S WI K III leasonable shape
02.3 92	LM02.3HAS	-	-	-	-
03 95 7	DM85 7DAS	-	-	-	-
63.1 96.25	RM05./RAS	-	-	-	-
80.55	RM60.55KDC	-	-	-	-
80.373	KM80.575KDC	-	-	-	-
Where.	RM = right margin		RS = rootwad sweeper		u/s = upstream
	MC = mid-channel		BP = brush pile		d/s = downstream
	LM = left margin		FC = floating crib		N/A - Not available
	C		PBL = pseudo beaver lodge		
			RAS = rail anchored sweeper		
			HAS = hand-placed anchored sweeper		
			PDC = pipe-pile debris catcher		
			RDC = rail debris catcher		
			DB = debris boom		
			SC= side channel		
			PB = point bar		
			PP = pocket pool		

Table B1b
Spring 1993 Assessment of Habitat Complexing Structures

Location	Site				
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
Reach 2					
15.6	LM15.6RAS	No	No	-	-
15.7	MC15.7PP	No	No	-	-
15.8	MC15.8PP	No	No	-	-
16.2	RM16.2RAS	Branches stripped	No	Fails to capture debris	-
16.5	RM16.5RDC	Shore deadman cable broken	No	Appears to have lost some debris	-
16.8	RM16.8RDC	No	No	Caught a few logs, very little small debris	-
17	RM17.0PB	No	No	-	Max. pool depth - 1.10 m
17.15	RM17.15PB	No	No	-	Max, pool depth - 1.14 m
17.3	RM17.3PB	No	No	-	Max pool depth - 1.30 m
17.9	RM17 9DB	No	No	Lots of debris on the shore	-
17.9	RM17.95C	No	No		_
10.2	L M19 2DDC	No	No	- Complex solid beeven lades	-
18.5	LMI8.5KDC	No	INO	Complex solid beaver lodge	-
20.65	RM20.65RDC	No	NO	Lots of debris	shear zone runs along outside of complex
21.3	LM21.3RDC	No	No	-	-
21.4	LM21.4RDC	No	No	Large log jam since construction	-
22	RM22.0RDC	No	No	-	-
22.1	RM22.1RAS	Cable very close to breaking	No	Fails to capture debris	-
22.55	RM22.55RDC	No	No	-	No visible flow, shear zone flows along outside of the complex
22.6	LM22.6RDC	No	No	Lots of debris on the shore	-
22.7	LM22.7RDC	No	No	-	_
22.85	LM22.85RDC	No	No	-	-
22.95	RM22.95RAS	No	No	-	-
23	RM23 0RDC	No	No	-	_
24.2	LM24 2RDC	No	No	-	Complex colonized by beavers
24.3	LM24 3RDC	No	No	_	
24.5	DM24.3KDC	No	No	-	-
24.55	PM24.55K5	No	No	-	-
24.4	DM24.4PC	No	No	-	-
24.0	RM24.0PDL	INO NI-	INO N-	-	-
24.8	RM24.8PBL	No	No	-	-
25.4	RM25.4RDC	No	No	-	-
25.7	MC25.7RDC	No	No	-	-
26.9	RM26.9RAS	No	No	-	-
27.4	RM27.4FC	No	No	-	Outside of complex floating
28.4	RM28.4RDC	No	No	-	-
29.4	LM29.4RAS	Sweeper broken at outer rail	No	-	-
31	RM31.0PBL	PBL frame broken	No	-	Debris compressed into a small bundle
31.1	RM31.1PBL	No	No	-	Debris shifted to d/s onshore corner of PBL frame
31.4	RM31.4BP	No	No	-	-
32.65	LM32.65HAS	No	No	-	-
34.7	RM34.7PDC	D/S pipe pile being lifted by	No	-	-
		ice, just about failing over			
35.4	MC35.4PDC	No	No	-	Filling in d/s of complex with weeds

and sediments

Table B1b
Spring 1993 Assessment of Habitat Complexing Structures

Spring 1993	3 Assessment (June	5 - 10, 1993): Discharge = 57.	5 - 59.5 m³/s (2,0	031 - 2,101cfs)	
Location	Site	_			
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
Reach 4					
72.9	LM72.9HAS	No	No	Debris added	Modified April 1993
73	LM73.0HAS	No	No	-	Swpr not modified due to lack of suitable anchoring and material
74.1	RM74.1HAS	Complex almost completely submerged	No	-	-
75.9	LM75.9HAS	No	No	Debris added	D/s sweeper added April 1993 to improve debris collection
78	LM78.0HAS	No	No	Debris added	-
80.2	LM80.2HAS	No	No	-	-
80.9	LM80.9RDC	No	No	-	High water flows over the top of rails
82.1	LM82.1RAS	No	No	-	-
82.2	LM82.2RAS	No	No	-	-
82.3	LM82.3HAS	No	No	-	-
83	LM83.0RDC	No	No	-	-
85.6	MC85.6RDC	No	No	-	Water flows over rails at high flows
85.7	RM85.7RAS	Branches reduced in size by beavers	No	Debris added	Repl.in Apr. 1993 and d/s boom added. Old sweeper rem. by ice
86.35	RM86.35RDC	No	No	Complex plugged with grasses and pollen	-
86.375	RM86.375RDC	No	No	-	-

Where, RM = right marginMC = mid-channelLM = left margin  $RS = rootwad \ sweeper$ 

BP = brush pile

FC = floating crib

PBL = pseudo beaver lodge

RAS = rail-anchored sweeper

HAS = hand-placed anchored sweeper

PDC = pipe-pile debris catcher RDC = rail debris catcher

RDC = rail debris c

DB = debris boom SC= side channel

SC- side channe

PB = point bar

PP = pocket pool

u/s = upstream d/s = downstream N/A - Not available

Table B2	
Fall 1993 Assessment of Habitat Complexing Structures	

Location	Site				
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
Reach 2					
15.6	LM15.6RAS	-	-	-	-
15.7	MC15.7PP	-	-	-	-
15.8	MC15.8PP	-	-	-	-
16.2	RM16.2RAS	-	-	-	-
16.5	RM16.5RDC	-	-	-	-
16.8	RM16.8RDC	-	-	-	-
17	RM17.0PB	-	-	-	-
17.15	RM17.15PB	-	-	-	-
17.3	RM17.3PB	-	-	-	-
17.9	RM17.9DB	-	-	-	-
17.9	RM17.9SC	-	-	-	-
18.3	LM18.3RDC	-	-	-	-
20.65	RM20.65RDC	-	-	-	-
21.3	LM21.3RDC	-	-	-	-
21.4	LM21.4RDC	-	-	-	-
22	RM22.0RDC	-	-	-	-
22.1	RM22.1RAS	-	-	-	-
22.55	RM22.55RDC	-	-	_	-
22.6	LM22.6RDC	-	-	-	-
22.7	LM22.7RDC	-	-	-	-
22.85	LM22.85RDC	-	-	_	-
22.95	RM22.95RAS	Sweeper broken in half	-	-	-
23	RM23.0RDC	-	-	_	-
24.2	LM24.2RDC	-	-	-	-
24.3	LM24.3RDC	-	-	_	-
24.35	RM24.35RS	-	-	-	-
24.4	RM24.4FC	-	-	_	-
24.6	RM24 6PBL	-	-	_	_
24.8	RM24.8PBL	-	-	_	-
25.4	RM25.4RDC	-	-	-	-
25.7	MC25.7RDC	-	-	_	-
26.9	RM26.9RAS	d/s boom broke	-	Major loss of debris	-
27.4	RM27.4FC	-	-	-	-
28.4	RM28.4RDC	-	-	-	-
29.4	LM29.4RAS	Sweeper broken in half	-	-	-
31	RM31.0PBL	-	-	-	-
31.1	RM31.1PBL	-	-	-	-
31.4	RM31.4BP	-	-	-	-
32.65	LM32.65HAS	-	-	-	-
34.7	RM34.7PDC	-	-	-	-
35.4	MC35 4PDC	-	-	_	_

Fall 1993 Assessment (November 19, 1993): Discharge = 32.7 m<sup>3</sup>/s (1,155 cfs)

Table B2	
Fall 1993 Assessment of Habitat Complexing Structures	

Location	Site				
(km)	Number	Damage	Displacement	Debris Accumulation/Loss	Recommendation/Comments
Reach 4					
72.9	LM72.9HAS	-	-	-	-
73	LM73.0HAS	-	-	-	-
74.1	RM74.1HAS	-	-	-	-
75.9	LM75.9HAS	-	-	-	-
78	LM78.0HAS	-	-	-	-
80.2	LM80.2HAS	-	-	-	-
80.9	LM80.9RDC	-	-	-	-
82.1	LM82.1RAS	-	-	-	-
82.2	LM82.2RAS	-	-	-	-
82.3	LM82.3HAS	-	-	-	-
83	LM83.0RDC	-	-	-	-
85.6	MC85.6RDC	-	-	-	-
85.7	RM85.7RAS	-	-	-	-
86.35	RM86.35RDC	-	-	-	-
86.375	RM86.375RDC	-	-	Significant debris capture	-
Where,	RM = right margin		RS = rootwad swee	per	u/s = upstream
	MC = mid-channel		BP = brush pile		d/s = downstream
	LM = left margin		FC = floating crib		N/A - Not available
			PBL = pseudo beaver lodge		
			RAS = rail-anchore	d sweeper	
			HAS = hand-placed		
			PDC = pipe-pile de		
			RDC = rail debris c	atcher	
			DB = debris boom		
			SC= side channel		
			PB = point bar		

Appendix C 1993 to 1995 Sketches of Habitat Complexes (As Built)

Appendix D

1993 to 1995 Habitat Complex Physical Assessment Photos



**Photograph 1:** Stable rootwad sweeper (RM24.35RS) providing 55 m<sup>2</sup> of cover area (May 1995).



Photograph 2: Brushpile (RM31.4BP) with little cover area due to mobile river bank (May 1995).



**Photograph 3:** Stable floating crib (RM24.4FC) showing large cover area of 91 m<sup>2</sup> (May 1995).



**Photograph 4:** Floating crib (RM27.4FC) not providing much cover as its upstream end pushed onto the shore (May 1995).



**Photograph 5:** Pseudo beaver lodge (RM24.6PBL) still retaining debris, providing 50 m<sup>2</sup> of cover area (May 1995).



**Photograph 6:** Pseudo beaver lodge (RM31.0PBL) removed from 1995 physical assessment due to loss of all debris (May 1995).



**Photograph 7:** Downstream boom added to rail anchored sweeper (LM82.1RAS) to improve debris capture (November 1993).



**Photograph 8:** Rail-anchored sweeper (LM29.4RAS) broken in half, stripped of majority of branches and not providing much cover area (November 1993).



**Photograph 9:** Downstream boom added to hand-placed anchored sweeper (LM75.9HAS) to improve debris capture (April 1993).



**Photograph 10:** Hand-place anchored sweeper (RM74.1HAS) reduced to bare log due to ice and summer flows. Removed from physical assessment in 1995 (May 1994).



**Photograph 11:** Smaller pipe-pile debris catcher (RM34.7PDC) providing 42 m<sup>2</sup> of cover area despite loss of downstream pile (May 1995).



Photograph 12: Large accumulation (149 m<sup>2</sup>) at pipe-pile debris catcher (MC35.4 PDC, May 1995).



**Photograph 13:** Rail debris catcher (RM86.375RDC) showing significant debris capture (November 1993).



**Photograph 14:** Rail debris catcher (MC85.6RDC) removed from 1995 physical assessment due to loss of all debris during summer cooling flows (May 1994).



Photograph 15: Stable debris boom (RM17.9DB) providing 60 m<sup>2</sup> of cover area (May 1995).



**Photograph 16:** Side channel (RM17.9SC) showing low water level, dewatered complexes and no velocity due to beaver dam blockage (May 1995).



Photograph 17: Stable point bar RM17.0PB showing shear zone (May 1995).



**Photograph 18:** Location of remaining pocket pool (MC15.7PP, May 1995). MC15.8PP removed from further physical assessment due to significant erosion..